Reply to Reviewer #1 comments on “Theoretical study of mixing in liquid clouds – Part 1: Classical concepts” by A. Korolev et al.

General comments to all three parts (repeated in all three reviews). I read the papers with considerable interest mostly because this seemed to be a popular topic some time ago, in both observations and modeling. I was curious to see what new these manuscripts bring. Frankly, I was disappointed. First, the analysis concerns a highly idealized problem, with little applications to real clouds. Turbulent mixing in clouds is by far more complicated that situations depicted in Fig. 1 of part 1 (and then repeated in different shapes as Figs. 1 in Part 2 and 3). Second, I am aware of study in which the authors developed a fairly sophisticated model of microphysical evolution during turbulent stirring (Jarecka et al., JAS 2013) aiming at prediction of the homogeneity of mixing. They applied the model to LES simulations of shallow convective cloud field. The impact was surprisingly small and the authors of that paper argued why this might be so (the entrained air comes from the descending shell and is not far from saturation). So in a sense the subject is “old news”. Finally, the lengthy discussions, full of unnecessary caveats and references to details of small multi-panel figures, made the reading frustrating. All three parts read like a student dissertation, not a concise scientific paper highlighting key points and leaving the rest for the reader to follow. Thus, I read the manuscripts with decreasing interest, and my comments are more detailed for the part 1, and get more general for parts 2 and 3.

Overall, I do not believe that the subject matter deserves close to 100 pages and close to 50 figures. I feel that the material deserves a single, short and concise manuscript, with new material clearly separated from what I feel has been discussed in the past, perhaps not at such a level of detail. Reading introductions to all three parts made me mad, because all three say basically the same thing with different language and organization. Part 1 is mostly trivial in my view, with some parts speculative and other repeating already published material (see detailed comments). Parts 2 and 3 have some aspects that perhaps deserve to be published, but it is not clear to me how useful these are (not very much in my opinion). References to aircraft observations are vague and missing the key aspect, which is the irrelevance of an idealized problem considered by the authors to low-spatial resolution observations of a complicated multiscale natural system.

Reply to general comments:
Authors appreciate the Reviewer’s time and efforts to review our manuscript. The overview sections, which were copied and pasted for all three different reviews, can be summarized by the following claims:

a) The problem of turbulent mixing in clouds “seemed to be a popular topic some time ago”, but now “the subject is old news”.

b) This study addresses a “highly idealized problem” and uses simplified models in order to describe cloud mixing.

c) The results presented in the papers are not new and are “repeating already published material”.

The authors strongly disagree with the above statements of Referee 1.

In response to the first claim: the mechanism of mixing is still not well understood and continues to be a highly relevant problem in the cloud physics community, especially given the high rate of recent publications on this topic. We believe that the three papers contribute significantly to the theory of interaction of cloud droplets with turbulent environment and
present novel techniques of investigating the effect of mixing both from a theoretical standpoint and through in-situ observations.

Second, in contrast to the reviewer, we support the common practice of using idealized models of complex cloud processes, in order to investigate physical mechanisms without being bogged down by the multitude of other processes involved. Idealized considerations (e.g. adiabatic assumptions) are widely used in cloud physics as well as in physics in general. The assumptions are clearly articulated at the beginning of each paper in order to let a reader judge about the level of idealization of the utilized approaches.

Third, as regards to novelty, the following new results have been obtained:

a) The first paper suggests a new technique for identifying type of mixing (homogeneous or inhomogeneous) based of the analysis of the moments of droplet size distributions. It was shown that homogeneous mixing breaks functional relationships between the moments. Nothing like that has been done before. A novel approach for identifying mixing from in-situ observations was proposed. The comments obtained by the authors from their colleagues showed that the proposed technique start to be utilized by other research groups.

b) The second paper considers homogeneous mixing. One of the important finding of this paper is an analytical universal solution describing the rate of evolution microphysical parameters as well as the final equilibrium state (mixing diagram). It is shown that in case of polydisperse droplet size distributions evolution of droplet spectra can lead to increase in characteristic size of droplets in contrast to widely accepted "classical" view, when the characteristic droplet size is decreasing. It was shown that evaporation time can be expressed in terms of time of phase relaxation. This is important for definition of reaction time in Damkoller number.

c) The third paper is dedicated to inhomogeneous mixing. A theoretical framework for a time dependent mixing of two volumes that accompanies by cloud droplet evaporation is developed. A new turbulence-evaporation model of time evolution of ensemble of droplets under different environmental parameters is proposed. In contrast to previous studies the Damkoller number is introduced as a result of re-normalization of mixing-evaporation equation, rather than empirically. It is shown that any mixing leads to droplet spectrum broadening. For the first time the scientifically grounded demarcation between homogeneous and inhomogeneous mixing in the space of environmental parameters is performed.

The authors regret that Referee 1 overlooked all these novelties.

The authors also believe it is impossible to follow the recommendation of Referee 1, to combine all papers into one single, summary paper. While the papers all consider the same subject, they perform completely different functions with regard to investigating the issues of mixing.

Comments:
A small technical comment: I think the terminology the papers use is not correct. The limiting cases should be referred to as homogeneous and extremely inhomogeneous mixing. Everything between the two is the inhomogeneous mixing.

Reply: Corrected. The term “inhomogeneous mixing” was changed to “extreme inhomogeneous mixing” throughout the text (~47 changes, see marked-up manuscript)
Specific comments to Part 1:
1. The title should include “concepts”, not “concept”.

   Reply: Corrected. The term “concept” was replaced by “concepts” in the title of the manuscript.

2. I feel the proper start to the discussion is to recognize that bulk properties (moist static energy and total water) are sufficient to calculate the final thermodynamic state (i.e., once the mixing is completed). However, the transformation of the droplet spectrum may lead to different spectra with the same final liquid water. Extremely inhomogeneous mixing leads to the final spectrum as given by (1), that is, number of droplets in each bin is simple reduced in the same proportion. Homogeneous mixing leads to a shift of the spectrum towards smaller sizes. In such a case, the shift may lead to a complete evaporation of the smallest droplets in the initial spectrum. Note that such a simple interpretation makes the first sentence in the abstract to the Part 2 trivial.

   Reply: The statements about independence of the final state of the bulk parameters on the type of mixing are scattered throughout the text of Part 1. One more statement was implemented in Section 2.1 following the reviewer’s comment (lines 134-140):
   “Based on mass and energy conservation considerations the final state of the bulk parameters (i.e. liquid water mixing fraction, humidity, temperature, etc.) is the same for both types of mixing. However, in the case of extreme inhomogeneous mixing saturation is reached through complete evaporation of some fraction of droplets, and their sizes remain constant. Whereas in case of homogeneous mixing saturation is reached through a uniform evaporation of droplets, and the total number of droplets remains unchanged. It should be noted, that in both cases the droplet concentration decreases due to dilution by the mixed droplet free sub-saturated parcel.”

3. The main problem with the observations is the insufficient spatial resolution. If the diluted cloud consists of filaments of cloud-free and undiluted cloudy air, averaging such a structure gives an impression of the extremely inhomogeneous mixing (this was pointed out long time ago, perhaps in one of the papers involving Charlie Knight). In fact, aircraft in-situ observations seldom allow looking at homogenized volumes, at least not at scales that the observations are able to resolve. Moreover, there are additional processes that affect droplet spectra, such as updraft and downdraft, activation of additional cloud droplets, collision/coalescence, etc.

   Reply: The problem here is not as much as in the particle probe resolutions, but rather in the identification of the stage of mixing. For example, Beals et al. (2015) demonstrated existence of cloud free zones in clouds down to cm scale. That’s the highest possible spatial resolution available nowadays. However, the results of this study and other similar studies do not provide answer, whether this is a final stage of mixing and the mixing is extremely inhomogeneous, or it is an interim stage of homogeneous mixing. To address this question collocated high spatial resolution (~1cm scale) measurements of temperature and humidity are required. Unfortunately, airborne instrument capable of such measurements are not available at that stage. The discussion about it was added in the text (lines: 604-616):
   “Strictly speaking the identification of type of mixing from particle probe measurements as it was performed in Sect. 5 is incomplete. It allows establishing correlation between microphysical moments and makes a formal conclusion about the mixing type, however it does
not allow judgement about stage of mixing (i.e. whether mixing is complete by reaching equilibrium). In most previous studies, including this one, identification of type of mixing was based on the assumption that the sampled cloud volume is in equilibrium state \((RH = 1)\), and that it reached the final stage of mixing (Fig.1 a2, a3, b3). It is possible that at the moment of measurement the process of mixing is not complete and the droplet free filaments remained undersaturated (Fig.1 a1, b1, b2). In this case the relationship between different moments may be well described as \(M_n = \alpha_{nk} M_{nk}\) and the mixing be confused with inhomogeneous mixing.

In order to identify stage of mixing, high frequency collocated measurements of temperature and humidity are required. Unfortunately current technology does not allow such measurements yet.”.

The discussion of the “non-mixing” processes (e.g. vertical velocity, WBF process etc.) affecting droplet size distribution was included in the original text. In the revised manuscript this discussion was shortened for the sake of conciseness (lines 621-635):

“Thus, collision-coalescence, riming or Wegener-Bergeron-Findeisen processes may change the droplet number concentration and liquid water content, and therefore, affect the relationship between the moments. Activation of interstitial CCN will result in breaking correlation between the moments due to formation of large concentration of droplets. Broad size distributions may also hinder identification of type of mixing due to partial evaporation of small droplets (Pinsky et al. 2015a)

It is anticipated that most suitable candidates to study mixing-entrainment process are non-precipitating convective clouds and stratocumulus clouds with relatively narrow droplet size distributions.

Another limiting factor is that the above consideration did not account for the effect of changing relative humidity in a vertically ascending parcel. Thus in droplet free entrained air \(RH\) increases approximately 10% for \(\Delta z = 200m\) at \(T = 0 \degree C\). After reaching saturation the mixing turns into a degenerate case, which will appear as extreme inhomogeneous mixing. Joint effects of evaporating droplets and an increase in \(RH\) during the vertical ascent may facilitate reaching saturation state. This case may also be relevant to the convective cloud described in Sect.5.2.”

4. Reference to Jarecka et al (JAS 2013) needs to be included in the paragraph starting at line 20 on p. 30213. Note that the review by Davenish et al. was published prior to that paper.

\textit{Reply:} The reference to Jarecka et al. was added (line 64).

5. Section 2.2. Figure 1 shows processes occurring at a constant volume. Does it make the difference that atmospheric processes typically take place at a constant pressure?

\textit{Reply:} Yes, it does. Consideration of the effect of pressure (e.g.\(u_z \neq 0\)) is not included in the text. This was stated in section 2.2. A potential effect of the vertical ascent was discussed in section 6. In the revised version this discussion was shortened compared to the original version (lines 630-636): “Another limiting factor is that the above consideration did not account for the effect of changing humidity in a vertically ascending parcel. Thus in droplet free entrained air relative humidity increases approximately 10% for \(\Delta z = 200m\) at \(T = 0 \degree C\). After reaching saturation the mixing turns into a degenerate case, which will appear as extreme inhomogeneous mixing. Joint effects of evaporating droplets and an increase in \(S\)
during the vertical ascent may facilitate reaching saturation state. This case may also be relevant to the convective cloud described in Sect.5.2.”

6. Section 2.3. Does the conservation of moist static energy and total water lead quickly to the answer?

*Reply:* The derivation of $\delta q$ was done based on the mass and energy conservation. Yes, it leads quickly to the answer for $q$ as long as mixing occurs in adiabatic volume. No changes were applied to the manuscript in regard to this comment.

7. I do not understand the statement below Eq. 9. Latent heating is included if one follows what I suggest in 6 above.

*Reply:* The mentioned statement is misleading and it was excluded from the text of the revised manuscript. The original meaning of this statement was to indicate that the temperature in Eq.9 in the original manuscript is used as a constant. The modified statement in the revised manuscript was moved to Appendix A (lines 694-697): “The process of evaporation is accompanied by changing humidity and temperature due to latent heat of vaporization. This process is described by the Eq. (C2) in Korolev and Mazin (2003). Assuming the process to be isobaric (i.e. vertical velocity $u_z = 0$) and absence of ice ($d q_i = 0$), Eq. (C2) (Korolev and Mazin, 2003) yields”

8. Section 2.4. The initial paragraph provides information that needs to be stated at the onset of the analysis (see 2 and 6 above).

*Reply:* The sequence of sections was rearranged in order to improve the flow of the text. The onset of the analysis is now provided in a new section 2.3 (“Effect of mixing on liquid cloud water and temperature”). The section on homogeneous mixing (original Section 2.4) is now described in Section 2.6. So, no onset is required in Sect.2.6 since it was all done in previous sections.

9. Eq. 15. The phase relaxation time scale goes back to Squires.

*Reply:* The reference to Squires was added (line 280).

10. Section 3. First, I do not think there is anything to model. Is the comparison between a specific model used by the authors (no details provided) and the analytical solutions the purpose of this section? Sections 3.1 to 3.4 should be compressed into a short section and a single figure should be selected. These sections are exactly what I mean by my statement that the paper reads like a student dissertation.

*Reply:* The main goal of section 3 is formulated as (lines 322-324): “Numerical simulations were performed to examine accuracy and limitations of the analytical expressions in Sect.2 and to conduct a sensitivity test to environmental and cloud parameters.” The authors consider that this section is important part of the manuscript to validate the equations and approach developed in sections 2.
A brief description of the model is provided at the beginning of section 3. “The simulations have been performed with the help of a parcel model similar to that in Korolev (1995). The ensemble of droplets in the simulation was assumed to be monodisperse. For the case of extreme inhomogeneous mixing the amount of evaporated water $\Delta q$ required to saturate the mixed volume was calculated first. If $\Delta q < \mu q_1$, then the concentration of evaporated droplets was calculated as $N_{ev} = \frac{\Delta q}{m_d \rho_a}$, where $m_d = \pi \rho_w D^3/6$. Then, the concentration of the remaining droplets $N = N_1 - N_{ev}$ was recalculated based on the calculation on the volume formed after mixing. If $\Delta q \geq \mu q_1$, then all droplets evaporate, and $N = 0$. For the case of homogeneous mixing in the first step the engulfed parcel instantly mixes with the cloud parcel resulting in a new humidity $RH_{m_0}$, temperature $T_{m_0}$ and volume $V_{m_0}$. After that the droplets start evaporating until either their complete evaporation or saturation over liquid is reached. The calculations stopped when, either $D < 0.2\mu m$ or $(E_S - e)/E_S < 0.001$, respectively.” This description is sufficient for cloud physicist to reproduce the results in section 3.

Section 3 were shortened and rearranged (see revised manuscript with ALL marked-ups). Figs.4-6 were converted into one figure as proposed by Reviewer.

11. Section 3.5 is perhaps a good start to a follow-up investigation. At the moment, it does not belong to this paper.

Reply: This section 3.5 was turned into section 4 in the revised manuscript. This section has a direct link to the subject of the paper, which might not be well articulated in the original text. The text of section 4 underwent significant modification to make it more clear. The purpose of this section is to demonstrate a breakup of functional relationships between the microphysical moments during progressive homogeneous mixing. This has a direct link to the subject of the paper, i.e. how microphysical moments are related to each other. A physical explanation of this phenomenon is also provided in the section 4 (new Fig.10). The results of this section help interpretation of in-situ observation (conceptual diagram in Fig.12) and explain broad scattering of data points in case of homogeneous mixing. This is specifically relevant to the past studies of mixing from in-situ observations.

12. Section 3.7. This is really not a summary.

Reply: The title of this section was renamed to “Expected relationships between the moments” (line 492). The text of the former section 3.7 was rewritten and moved into Sections 5.1 in the revised manuscript.

13. Section 4 is long and does not bring anything new in my view. What is the point of having it here? I was not able to follow detailed discussion in section 4.1 and references to the specific figures. Section 4.2 can be omitted. I question the link between in-cloud observations and the results of theoretical analysis that the previous sections provide.

Reply: Section 4 (“In-situ observations”) in the original manuscript is changed to Section 5 in the revised manuscript. This section demonstrates how the results obtained in sections 2, 3 and 4 can be utilized for identification of mixing type from in-situ observations. This is a logical continuation of the theoretical study started at the beginning of the manuscript, which
ended by demonstration of its application to cloud measurements. The novel results in this section are: (1) the scattering diagrams of homogeneous and inhomogeneous mixing in Fig.12; (2) demonstration of utilizing the new approach for identification of type of mixing. Most of the previous studies to identify homogeneous mixing were based on the comparisons of measurements with the $N - r_v$ calculated for the first stage of mixing. Such attempts have a limited success and in many ways may be misleading. This section demonstrates utilization of other moments, which makes identification of type of mixing more robust.

Section 4.2 was shortened and some of it parts moved to section 6 “Discussion”. It bring up a warning that utilization of the developed approach for identification of type of mixing has limited capability and that it should not be blindly applied to a random cloud.

14. Section 5 discusses aspects that have been beaten up in other papers. Just a short paragraph with proper references would be sufficient.

Reply: The entire section on time scales was removed in the modified manuscript to make the paper more focused on the relationships between the microphysical moments.

15. Conclusion section is short, perhaps not surprisingly.

Reply: Nothing to comment.
Reply to Reviewer #2 comments on “Theoretical study of mixing in liquid clouds – Part 1: Classical concepts” by A. Korolev et al.

Overview:
The main contribution of this paper apparently is to demonstrate the relationship between different moments of the size distribution for the limits of homogeneous and extreme inhomogeneous mixing. Analytical results are compared with the results from a parcel model. The conceptual picture of inhomogeneous and homogeneous mixing is well illustrated in Figure 1 and the central analytical expression is validated in Figure 2. Figures 3-8 then show the response of different moments of the cloud droplet size distribution to idealized mixing processes. Figures 9-11 describe a conceptual model of a cascade of mixing events between a dry parcel and the cloud, which is a step toward making comparisons between the theory and observations within an evolving cloud environment. Section 4 and Figures 12-15 provide a brief analysis of observational data in the context of the conceptual models developed in the previous sections. The analysis is useful in attempting to connect the concepts and idealized models to the more complex situation observed in real clouds. The paper ends with a discussion of characteristic time scales, which seems somewhat disconnected. It is not clear how this integrates with the previous sections, and perhaps it should be either moved closer to the introduction or separated as an appendix. If kept in this location, its logical flow with the rest of the paper needs to be improved. Overall, my sense is that the expanded view to consider different moments of the size distribution is a valuable contribution, especially for the experimental cloud physics community, but perhaps also for applications to radiative transfer, remote sensing, etc. I am not aware of other papers where different moments are considered thoroughly as here, so this seems to be original. Comment regarding disconnect of the section 5 discussing the characteristic time scales.

Reply: Authors highly appreciate the Reviewer’s comprehensive comments and time to read our manuscripts. Special thanks for thoroughly going through equations and revealing numerous typos.

The manuscript underwent major revision and modification. The text was shortened to make it concise, sections were rearranged, some of them were re-written, the variable names were modified to be consistent with part 2 and 3. We agree that Section 5 is in many ways disconnected, and it was excluded from the manuscript.

General criticisms:
1. The application to size distribution moments is original, as far as I am aware (Jeffery gave a brief discussion of how the second moment is affected by mixing, but the treatment here is much more thorough and covers all typical moments). But much of the conceptual model is written more like a textbook. Maybe this is nice for readers new to the field, but the authors take a risk in expanding the length of the paper, especially when combined with the other two parts. Much more important, and definitely missing from the introduction as it currently stands, is some kind of overview of how the three part series fits together. What are the different levels of complexity treated? Why are two specialized papers on homogeneous and inhomogeneous mixing needed if part 1 already treats both cases? Now that I have read all three parts I have an idea, but this needs to be clear from the outset. It is especially important to motivate why part 1 should be connected at all. Currently it is disconnected in its approach, in its use of observational data, and even in its notation. The use of observational data is nice, but it is somewhat confusing given the title “theoretical study…” The notation is a major problem that needs to be corrected… the physics is difficult enough by itself, without having to translate symbols from one paper to the next.
Reply: The authors shortened several pages of the text in order to reduce the size of the manuscript and make it concise. A number of cross references were added in all three parts in order to link them together. As it is seen now, part 1 is closely related to part 2 and it uses the same approach. Part 3 utilizes the results of part 2. The first part uses experimental data to demonstrate the how the theoretical outcomes could be verified from in-situ measurement. In our opinion such comparisons with experimental results are natural, and if it is not there, it probably might be requested by reviewers.

We also checked Jeffery’s works on mixing. However, no discussions of the effect of mixing on the DSD second moment were found. We appreciate, if this reference could be provided.

2. After a long preliminary discussion, the most important paragraph in the introduction is on page 30214 starting at Line 26: “Besides the effect on N and r the type of mixing is anticipated to manifest itself in relationships between other moments of the droplet size distribution…” It should be further explained in that paragraph why it is valuable to analyze different moments. Are they expected to be more insightful than the traditional mixing diagram methodology; is it making applications of mixing to other fields clearer; etc?

Reply: The paragraph explaining importance of the effect of mixing on the DSD moments was added in the introduction following the Reviewer’s comment (lines 102-106): “It is shown that the newly obtained relationships between the moments provide a more robust identification of type of mixing from in-situ measurements as compared to conventional N − D^3 relationships used in mixing diagrams. Relationships between moments may be useful for parameterization of mixing in numerical simulations of clouds and climate, interpretations of remote sensing measurements.”

3. In Fig. 9 and after, a multiple-step mixing process is envisioned. The approach is to consider mixing between a cloud and the dry environment, and then to consider subsequent mixing events between that parcel and the cloud again. Why did the authors choose to take this view instead of considering a cloud parcel progressively mixed with clear air? Some motivation for that choice is needed and some discussion of how the results would be expected to differ. For example, if one were to focus on the dry air first, dots should be concentrated at lower end in Figure 10.

Reply: The modeling of the progressive mixing presented in the paper corresponds to the case when the entrained dry air is interacting with the cloudy environment. The final state of this interaction is a diluted cloud. The progressive mixing of the cloud environment with the environmental dry air corresponds to detrainment, which ultimate state is dry cloud free air. It can be show that during detrainment the relationships between moments will be the same as during primary mixing. The authors consider that the case of detrainment is less interesting, and left it outside the frame of the manuscript in order to keep it concise. However, following the reviewers suggestion a paragraph was added in the revise manuscript in order to explain the motivation of our choice (lines 455-460): “It is worth noting that progressive mixing with the dry air does not break the functional relationships between the moments. This case is equivalent to detrainment of cloudy environment into dry air. It can be shown that Eq.(14) remain valid at any stage of progressive homogeneous mixing with dry air only, i.e.
\[ \frac{N_j}{N_1} = \mu^{(1)} \cdots \mu^{(j-1)} \mu^{(j)} \] where \( \mu^{(j)} \) is the mixing fraction at the \( j \)-th stage of mixing. Eqs. (15)-(24) also remain valid for the progressive mixing with the dry air only.

4. There are many mistakes in the paper, including errors in the equations, at least according to the derivations as I am able to follow them. Again, the physics is difficult enough by itself, without having to make corrections. Please thoroughly check all results and the typesetting.

*Reply:* The authors highly appreciate the Reviewers efforts to improve our manuscript and pointing out numerous typos. All specific comments listed below were addressed and the text of the manuscript was thoroughly checked.

**Specific comments**

1. Eq. 1, page 30218: As monodisperse cloud droplets are used in this part of the study, the droplet size distribution \( f(r) \) will confuse people. Especially Equations 2 and 3 only work for monodisperse droplets theoretically. Please explain and be consistent.

*Reply:* The relationships between moments are valid for relatively narrow polydisperse droplet size distributions. However, the modeling was performed for monodisperse size distributions. The confusion about assumption of monodisperse droplets during deriving relationships between the moments is probably coming from mentioning monodisperse size distributions in section 2.2. The statement about the assumption of monodispersity was removed from section 2.2 to avoid confusion.

2. Eq. 5: prefactor should be \((cpRvTmo^2/L^2)\)? Tmo not T2?

*Reply:* The prefactor was corrected in the revised manuscript in Eq. (2), (former Eq.5).

3. It is difficult to connect Eq. 8 to Eq. 5. How do you prove Eq. 5 is \((1-\mu)\) Eq.8, when \( T_1=T_2=T_{mo} \)?

*Reply:* The term \((1-\mu)\) appears as a result of expansion in series. Appendix B was added to clarify the derivation of this equation.

4. Line 21, page 30218: q is liquid water mixing ratio (g/kg), not liquid water content (g/m3).

*Reply:* Corrected: line 251 in the revised manuscript.

5. Line 6, page 30220: The neglect of latent heat is a strong assumption that removes possible important factors such as negative buoyancy production. It is valid in the range specified by the authors, but the limitation should be discussed. Does it restrict the results to certain environments or cloud types (e.g., shallow convection)?

*Reply:* If fact the latent heat was accounted during derivation of Eq.3 (old Eq.8) (see Eq.A7 in Appendix A). The confusion regarding disregarding the latent heat is coming from inaccurate statement on page 30220 as indicated by Reviewer. The original purpose of this statement was to indicate that the temperature is included as a coefficient and it remains constant. In order to address the Reviewer’s concern the calculation of temperature during mixing was added in the text (line 217-219): “The temperature at the final stage of mixing can be estimated as (appendix C)”
\[ T = T_{m0} - \frac{(1-\mu)\delta q^* L}{c_{pa}}, \quad \text{when} \ \mu > \mu_{cr} \]  

(6a)

\[ T = T_{m0} - \frac{\mu q_1 L}{c_{pa}} \quad \text{when} \ \mu \leq \mu_{cr} \]  

(6b)

In order to demonstrate that \( \delta q^* \) and \( \delta q_m \) allow accurate depiction of the temperature depression during mixing-evaporation process, the air temperature formed after mixing calculated from Eq. 6a,b was compared with the modelled temperature in Figs. 4h and 6h.

   
   Reply: Corrected: line 208 in the revised manuscript.

7. Line 13, page 30220: missing space between “on” and “delta_q”
   
   Reply: This sentence was deleted in the revised manuscript.

8. Line 17, page 30220: the volume change due to temperature change should not affect liquid water mixing ratio, because it’s connected to mass not volume as mentioned in point 4.
   
   Reply: This paragraph was deleted.

9. Eq. 8: prefactor should be \((cpRvT^2/L^2)\)?
   
   Reply: The prefactor was corrected in the revised manuscript in Eq.(4) (former Eq.8).

10. Eq. 13: left side should be \(r^{33}/r^{303}\)
    
    Reply: Corrected: Eq.16a in the revised manuscript.

11. Eq. 14b: I think the right side should be \((q/q_0)^{2/3}(q+\delta q^*/q_0+\delta q^*^{*})^{1/3}\)
    
    Reply: Corrected: Eq.17b in the revised manuscript.

12. Eq. 16: I believe the exponent should be -1/3, and inside the parentheses should be \(N_0/N\).
    
    Reply: Corrected: Eq.18 in the revised manuscript.

13. Eq. 20: right side should be \(q^{2/3}(q+\delta q^*)^{1/3}/q_0\)
    
    Reply: Corrected: Eq.21 in the revised manuscript.

14. Fig. 3: it looks like panels a and b are mixed up. Also the caption refers to liquid water mixing ratio but the axis label states LWC; needs to be consistent.
    
    Reply: Figure 3 labeling was corrected as per Reviewer comment.

15. Figs. 3 and 4: should use same format for S through the whole paper (e.g. 20% as in Fig.4 or 0.2 as in Fig. 3)
    
    Reply: Corrected. In the revised manuscript \(S\) is replaced by \(RH\) in order to address the earlier Reviewer’s comment regarding consistency of notations with part 2 and 3. \(RH\) is determined as a saturation ratio ans the \(RH\) units were adjusted throughout the text.

16. Lines 12-15, page 30224: Lots of problems here. Where are the black stars in Fig. 4? Do you mean the stars in panels (a) and (b) of Figure 3, or should there be stars in Figure 4 too? And by the
way, the stars in Figure 3 are very difficult to see... I had to search for them. And again, regarding text on line 14, the question of LWC versus q comes up. Finally, on line 15 it is not obvious to be that the statement is for Figs. 3 and 4. Do you mean to include Fig. 2 also?

Reply: Figure 4 (former Figure 3) was modified to address the Reviewer’s comment. The critical mixing ratio now is indicated on all diagrams (a-h). The associated text was modified to make it consistent with the diagrams (lines 234-237): “Figure 2 shows comparisons of dependences of $\mu_{cr}$ vs. $q_1$ calculated from Eq. (7) and those deduced from a numerical model (Sect. 3). Critical mixing fraction $\mu_{cr}$ is also shown by black stars in Fig. 4. The locations of the stars in Fig.4 coincide well with the locations, where the modeled microphysical moments become zero.”

17. Line 25, page 30226: q0 is not liquid water content.
   Reply: Corrected: line 369 in the revised manuscript.

18. Line 9 page 30227: Fig.17 should be Fig. B1?
   Reply: Corrected: Figure A1 in the revised manuscript.

19. Fig. 7: why changes from $r_0=10\,\mu$m (Fig. 4,5,6) to $r_0=5\,\mu$m. And also changes the S from 50% to 90%?
   Reply: The sizes 10$\,\mu$m and 5$\,\mu$m were selected to demonstrate mixing for the cases $T_1 = T_2$ and $T_1 \neq T_2$ in a most pronounced way. For the case RH$_2=50\%$ no supersaturation will be formed. Positive supersaturation may occur only at RH$_2>80\%$ and $\Delta T<15^\circ$C. Larger $\Delta T$ seems to be uncommon for the tropospheric clouds.

20. Fig. 8: My understanding is that homogeneous and inhomogeneous mixing coincide with each other for Smo>1? It’s hard to see this phenomenon in Fig. 8 (might use different colors or symbols?) also line 5 page 30228: unclear, should be “exceed those for inhomogeneous mixing for delta_T=0 and delta_T=5...?”
   Reply: Corrected: In the revised manuscript in Fig.7 (former Fig.8) inhomogeneous mixing for $\Delta T=10^\circ$C is indicated by the grey circles and it coincides with the line for homogeneous mixing. For $\Delta T=0^\circ$C homogeneous mixing line never crosses the extreme inhomogeneous line. For $\Delta T=5^\circ$C this section is not resolved in Fig.7 due to it proximity to point (1,1). In order to clarify this issue the following text was added (lines 398-401): “However, no activation of new droplets during isobaric mixing was allowed in this study. For the cases when RH$_{m0} > 1$ (Fig. 7, AB on line 1) the condensed water was uniformly distributed between available droplets. Therefore, $q(N), \beta(N)$ and $D_v(N)$ calculated for homogeneous and extremely inhomogeneous mixing coincide with each other on this interval.”.

21. Line 5, page 30228: in Fig. 8, Delta_T is negative, here it’s positive.
   Reply: The associated sentence was deleted in the revised manuscript.

22. Line16, page 30228: could you explain why “the effect is more pronounced when $T_1>T_2$ compared with $T_1<T_2$.”
   Reply: When the entrained air is colder ($T_1>T_2$), it results in additional condensation of the cloudy air due to its cooling compared to the case when the dry air is warmer ($T_1<T_2$). This
statement is supported by the results of numerical simulations. This explanation was not included in the text for the sake of conciseness.

23. Line 27, page 30229: “becomes denser towards the top right corner” Is it because the mixed volume is mixed with cloud volume, not environmental volume?
   \textit{Reply:} Yes. The mixing with the cloud environment results in approaching of the properties of mixing environment to the cloud properties. Eventually the entrained air is dissolved in the cloudy environment. Again, for the sake of brevity we did not expand this explanation in the manuscript.

24. Fig. 11: why use r0=5 um, not 10 um. It’s better to use the same radius through the paper, except you want to do the sensitivity test.
   \textit{Reply:} During the paper preparation the authors tried different \( r_0 \). Unfortunately is does not work well for the same \( r_0 \). Different \( r_0 \) (5\( \mu \)m and 10\( \mu \)m) were used in order to demonstrate the most pronounced effect of mixing on microstructure. A relevant comment was embedded in the text to address this issue.

25. Line 13, page 30231: missing space between “q” and “beta”
   \textit{Reply:} Corrected: line 498 in the revised manuscript

26. Line 14, page 30231: define Sc, Ac, Cu, Cb
   \textit{Reply:} This sentence was deleted in the revised version.

27. Line 1, page 30232: missing space between “N” and “q”
   \textit{Reply:} Corrected: line 509-510 in the revised manuscript

28. Fig. 13: caption T=12 not -120
   \textit{Reply:} The caption to Fig.13 is corrected

29. Line 13, page 30233: how does sample averaging affect homogeneous versus inhomogeneous mixing?
   \textit{Reply:} This is a good question. It was debated over years: how the averaging scale affects identification of the type of mixing, i.e. homogeneous versus inhomogeneous? The single instrument approach used in this and the majority of previous studies does not allow judgement about type of mixing at scales smaller than the averaging scale \( L_{av} \). In part 2 it was shown that for typical cloud environmental conditions the upper spatial scale of homogeneous mixing is limited by few m. Inhomogeneous mixing depending on the conditions may cover a wide range of scales from cm to km. A discussion of spatial scales of homogeneous and inhomogeneous mixing is provided in parts 2 and 3. Another question related to in-situ observations is whether the mixing reached equilibrium state at the moment of measurement.

30. Fig. 14a: y axis unit (g/m3) not (km-1)
   \textit{Reply:} The y-axis label in Fig.14a was corrected following the Reviewer comment.

31. Fig. 14: what’s the dash line in a,b,d
   \textit{Reply:} The explanations for the dashed lined was implemented in the caption for Fig.14 (line 892): “Dashed lines are linear regressions.”
32. Line 9, page 30237: Da>>1 is for inhomogeneous mixing, while Da<<1 is for homogeneous.
   
   Reply: This section was removed in the revised manuscript.

33. Line 14, page 30237: Andrejczuk is misspelled both here and in the reference list.
   
   Reply: Corrected: lines 64, 749

34. Lines
35. Lines 17-22, page 30238: lambda_ev, lambda_v, and lambda_DeltaV need to be defined, and the assumptions in calculating them clarified (e.g., evaporating distance assumes droplet always falling at terminal speed corresponding to time-dependent radius?).
   
   Reply: This section was removed in the revised manuscript.

36. Line 6, page 30240: S2 approximate 1 not 0?
   
   Reply: This section was removed in the revised manuscript.

37. Line 6, page 30240: missing space between “concentration” and “nev”
   
   Reply: This section was removed in the revised manuscript.

38. Fig. 16: define A and B in the text or caption
   
   Reply: This section was removed in the revised manuscript.

39. Line 13, page 30240: missing space
   
   Reply: This section was removed in the revised manuscript.

40. Line 15, page 30240: missing space
   
   Reply: This section was removed in the revised manuscript.

41. Eq. B4: left side should be Tmo not Tm
   
   Reply: Eq.A4 (former Eq.4B) was corrected to address the Reviewer comment.

42. Eq. B8: There seem to be mistakes here. I believe the prefactor should be (cpRvTmo2/L2) and Tmo not T2?
   
   Reply: Eq.A8 (former Eq.B8) was rewritten so the prefactor is in included in coefficient a (lines 701-704):
   
   \[
   \delta q_m = -b \ln \left( \frac{1 + aR_H_{m0}}{1 + a} \right) \tag{A8}
   \]

   the mixing ratio of liquid water required to evaporate in order to saturate 1kg of the cloud volume formed after mixing with the entrained air, but before droplet start evaporating. Here

   \[
   a = \frac{E_b R_q L^2}{p_c p_v \tau_{m0}} , \quad b = \frac{c_p R_v^2 \tau_{m0}^2}{v^2} .
   \]

43. Line 14, page 30244: “is hold” should be “holds”?
   
   Reply: Corrected following the reviewer comment: line 708 in the revised manuscript
44. Line 15, page 30244: Figure B1 is Figure 17.
   *Reply:* Figure A1 numbering was corrected to address the Reviewer comment

45. Table A1: there are two `tao_ev`
   46. *Reply:* The variable related to the time scale section were removed from the table.
Theoretical study of mixing in liquid clouds. Part 1: classical concepts

(revised version, 14 March 2016)

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Abstract

The present study considers final stages of in-cloud mixing in the framework of classical concept of homogeneous and extreme inhomogeneous mixing. Simple analytical relationships between basic microphysical parameters were obtained for homogeneous and extreme inhomogeneous mixing based on the adiabatic consideration. It was demonstrated that during homogeneous mixing the functional relationships between the moments of the droplets size distribution hold only during primary stage of mixing. Subsequent random mixing between already mixed parcels and undiluted cloud parcels breaks these relationships. However, during extreme inhomogeneous mixing the functional relationships between the microphysical parameters hold both for primary and subsequent mixing. The obtained relationships can be used to identify the type of mixing from in situ observations. The effectiveness of the developed method was demonstrated using in-situ data collected in convective clouds. It was found that for the specific set of in-situ measurements the interaction between cloudy and entrained environments was dominated by extreme inhomogeneous mixing.
1 Introduction

Turbulent mixing is an important non-adiabatic process in the atmosphere that to a large extent determines spatial gradients of many thermodynamic (e.g. temperature, humidity) and cloud microphysical parameters (e.g. hydrometeor concentrations, extinction coefficient, condensed water content) and as such, needs to be properly described in numerical simulations of clouds and weather predictions. Entrainment and mixing occurs during the entire lifetime of a cloud and is active not only near cloud edges, but it is important throughout the whole cloud volume. Mixing of cloudy and entrained air results in changes to the shape of the droplet size distribution through partial droplet evaporation and can also lead to changes in droplet concentration through complete evaporation of some fraction of droplets and dilution. The shape of the droplet size distribution plays key role in the initiation of precipitation and radiative properties of clouds.

The treatment of mixing in numerical simulations of clouds and precipitation formation remains a challenging problem. Besides the issues related to the way to describe mixing in numerical schemes, there is a fundamental problem of identifying a scenario or path, that mixing events should follow. Through the pioneering works of Latham and Reed (1977) and Baker et al. (1980) two explicitly alternative scenarios of mixing were identified. In the first scenario turbulent mixing rapidly stirs the environment homogenizing the fields of temperature and humidity. Following that, all of the droplets undergo partial evaporation under the same conditions. The result of this mixing is a droplet population with reduced sizes, but a total number that remains unchanged. This type of mixing is referred to as \textit{homogeneous}. In the second scenario mixing occurs more slowly such that the population of droplets experiences different amount of sub-saturation. Some number of droplets completely evaporates, while others experience no evaporation until the entirety of the entrained air becomes saturated. Following that, turbulence mixes the rest of the droplets with the saturated, but droplet-free environment. During this type of mixing the size of droplets remains unchanged; however, their total number is reduced. This type of mixing is called \textit{extreme inhomogeneous}. The intermediate case when some fraction of droplets evaporates partially, another other fraction evaporates completely, and a third fraction remains unchanged is in some works referred to as inhomogeneous (e.g. Baker and Latham, 1980).

The conditions for homogeneous and \textit{extreme inhomogeneous} mixing and their effects on precipitation formation have been debated in cloud physics over forty years. There are a number of numerical simulations and theoretical efforts on studying different aspects of mixing and its effect.
on cloud microphysics (e.g. Baker and Latham, 1982; Jensen and Baker, 1989; Su et al., 1989; Lasher-Trapp et al., 2005; Jeffrey, 2007; Andrejczuk et al., 2009; Kumar et al., 2013; Jarecka et al., 2013; and many others). A comprehensive review of the works on the effect of turbulence and mixing on cloud droplet formation can be found in Devenish et al. (2012).

A number of studies were dedicated to identifying type of mixing based on in-situ observations. Most of the previous observations provided evidence supporting inhomogeneous mixing (e.g. Hill and Choularton, 1985; Paluch, 1986; Bower and Choularton, 1988; Blyth and Latham, 1991; Gerber et al., 2008, Lu et al. 2011; Beals et al. 2016). However, works of Jensen and Baker (1989), Paluch and Baumgardner (1989), Burnet and Brenguier (2007), Lehmann et al. (2009), Lu et al. (2011) suggested occurrence of homogeneous mixing. So, at the moment it appears that both types of mixing may occur in liquid clouds. However, the environmental conditions governing one or the other type of mixing remain not well understood.

Early experimental work on identifying type of mixing from in-situ observations were based on the analysis of spatial variability of the shapes of individual droplet size distributions (e.g. Paluch and Knight, 1984; Paluch, 1986; Bower and Choularton, 1988). The effectiveness of this method involving the analysis of a large number of individual size spectra turned out to be quite low. Another technique utilized expected functional relationships between droplet concentration ($N$) and droplet diameter ($D$) specific to each type of mixing. Thus, during extreme inhomogeneous mixing the droplet size is expected to remain unchanged, whereas the concentration will vary. During homogeneous mixing the droplet size and concentration in cloud will be related to each other in a certain way, depending on the mixing fraction and the humidity of the entrained air. This fact was used in observational studies for identifying the type of mixing from “mixing diagrams” that related $N$ and $D_v$ for different regimes of mixing (e.g. Burnet and Brenguier, 2007; Gerber et al., 2008; Lehmann et al., 2009).

The use of mixing diagrams to some extent facilitated identification of type of mixing. However, in many cases scatter in the relationships between $N$ vs. $D_v$ was too large, hindering identification of the type of mixing (Burnet and Brenguier, 2007). To resolve this problem many researchers used other complementary measurements supporting identification of the type of mixing (e.g. Gerber et al., 2008; Lehmann et al., 2009).

Besides the effect on $N$ and $D_v$, the type of mixing is anticipated to manifest itself in relationships between other moments of the droplet size distribution, $f(D)$. Such relationships may
provide insight into the mixing process and identify type of mixing. With the exception of the work by Hill and Choularton (1985), who correlated concentration and liquid water content, there have been few attempts to use any other microphysical parameters for identification of type of mixing.

In order to fill this gap, this study presents a theoretical analysis of relationships between different moments of $f(D)$ within the framework of homogeneous and extreme inhomogeneous mixing. The analysis is focused on the first four moments of $f(D)$ corresponding to the droplet concentration $N$ (0th moment), integral diameter $N\bar{D}$ (1st moment), extinction coefficient $\beta$ (2nd moment), liquid water mixing ratio $q$ (3rd moment) and mean volume diameter $D_v$ (mixed 3rd and 0th moment). It is shown that the newly obtained relationships between the moments provide a more robust identification of type of mixing from in-situ measurements as compared to conventional $N - D_v^3$ relationships used in mixing diagrams. Relationships between moments may be useful for parameterization of mixing in numerical simulations of clouds and climate, interpretations of remote sensing measurements.

This paper constitutes the first in a series of three papers. It considers the final stage of mixing based on the formal definitions of homogeneous and extreme inhomogeneous mixing. These two types of mixing present two extreme regimes of mixing. The following two papers provide a detailed analysis of the time dependent processes during homogeneous (Pinsky et al., 2016a) and inhomogeneous (Pinsky et al., 2016b) mixing where non-extreme regimes are considered as well.

This paper is arranged in the following way. Section 2 presents analysis of the analytical relationship between $N, N\bar{D}, \beta, q, D_v$ and mixing fraction $\mu$ for the cases of homogeneous and extreme inhomogeneous mixing. In Sect. 3 the obtained analytical relationships are compared with the results of numerical simulation of $N, \beta, q, D_v$ formed at the final stage of mixing. Section 4 presents results of simulation of progressive mixing and its effect on the relationships between moments. Examples of relationship between $N, \beta, q$ and $D_v$ from in-situ observations are presented in Sect. 5. The discussion and concluding remarks are presented in Sect. 6 and 7.

2 Effect of mixing on microphysical variables

2.1 Phenomenological consideration

The conceptual diagrams of homogeneous and extreme inhomogeneous mixing are shown on Fig. 1. During the first stage of extreme inhomogeneous mixing the subsaturated parcel is engulfed
into the cloudy environment (Fig. 1a1). Then, the droplets at the interface of the sub-saturated parcel and the cloud environment undergo complete evaporation until the air within the engulfed volume reaches saturation (Fig. 1a2). After that the saturated but droplet free parcel mixes with the rest of the cloud environment (Fig. 1a3). The result of inhomogeneous mixing is that the cloud parcel has reduced droplet concentration and the droplet sizes remain unchanged.

In the case of homogeneous mixing after entraining into a cloud (Fig. 1b1), the subsaturated parcel “instantly” mixes up with its cloud environment (Fig. 1b2) leading to undersaturation of the total volume. Then, all droplets throughout the mixed volume undergo simultaneous evaporation until the equilibrium state is reached. The result of homogeneous mixing is a cloud volume with reduced concentration of droplets and droplets with reduced sizes (Fig. 1b3).

Based on mass and energy conservation the final state of the bulk parameters (i.e. liquid water mixing fraction, humidity, temperature, etc.) is the same for both types of mixing. However, in the case of extreme inhomogeneous mixing saturation is reached through complete evaporation of some fraction of droplets, and their sizes remain constant. Whereas in case of homogeneous mixing saturation is reached through a uniform evaporation of droplets, and the total number of droplets remains unchanged. It should be noted, that in both cases the droplet concentration decreases due to dilution by the mixed droplet free sub-saturated parcel.

The following discussion will be specifically focused on the microphysical properties formed at the final stage of the homogeneous and extreme inhomogeneous mixing. The processes occurring during mixing state (i.e. transition 1a→2a and 1b→2b in Fig. 1) remain outside the frame of this work. Following the formalism of homogeneous and extreme inhomogeneous mixing, the process of mixing reaches the final stage when (1) the entrained and cloud environment are mixed up and the spatial gradients of the microphysical ($N$, $\beta$, $q$, etc.) and environmental ($T$, $S$, $e$, etc.) parameters approach to zero; (2) the diffusional process related to droplet evaporation comes into equilibrium. The second condition is completed when (a) the environment reaches saturation state, or (b) the entire population of droplets is completely evaporated, if the entrained air is sufficiently dry.

The above description of homogeneous and extreme inhomogeneous mixing is highly idealized. Actual in-cloud mixing does not occur as a sequence of discrete events (Fig.1) that individually come to equilibrium only to be followed by next discrete mixing events. But rather it is occurring continuously on a cascade of different spatial and time scales. Broadwell and Breidenthal (1982) summarized the experimental evidence and proposed the following description
of mixing in turbulent shear layers. Mixing takes place in a series of events. Two shear layers exchange mass by engulfing parcels from an opposite layer into localized zones. The initially large-scale filaments of the two gases break down towards smaller scales due to the action of turbulence. The turbulence stretches the interface between the gases and enhances the molecular diffusion across the increasing surface. The actual mixing of the engulfed volume is a molecular diffusion process that is most effective after the break down volumes reduce to the Kolmogorov viscosity scale. It is anticipated that the reaction of the ensemble of droplets is a combination of homogeneous and inhomogeneous mixing with domination of one type of mixing over the other depending on the characteristic spatial and time scales of the environment determined by turbulence, cloud microphysics, state parameters and stage of mixing.

2.2 Methodology

The foregoing discussion will be focused on mixing between saturated cloud parcels and out-of-cloud sub-saturated air. The cloud parcel contains droplets with average diameter \( \bar{D}_1 \), liquid mixing ratio \( q_1 \) and number concentration \( N_1 \). The initial temperature in the cloud parcel is \( T_1 \), relative humidity \( RH_1 = 1 \), where \( RH = e / e_s(T) \) (the explanation of variable notations is provided in Table 1). The second parcel is droplet free \( (N_2 = 0) \), sub-saturated with initial relative humidity \( RH_2 < 1 \) and temperature \( T_2 \). The mixing occurs isobarically, i.e. \( p = \text{const} \). At the final stage of mixing the temperature and humidity formed in the resulting parcel are \( T \) and \( RH \) (appendix A). The process of mixing is completed when the mixed parcel reaches equilibrium due to the air saturation (i.e. \( RH = 1 \),) or due to the complete evaporation of droplets. In the latter case the final humidity is \( RH \leq 1 \). The effect of the vertical velocity and vertical travel on final \( T, RH, \) and \( q \) is not considered here, i.e. vertical velocity \( u_z = 0 \).

Without the loss of generality the masses of the cloudy and sub-saturated volumes prior to the mixing are assumed to have a unit masses, i.e. \( m_1 = 1 \) and \( m_2 = 1 \). The mixing process will be considered as mixing of \( \mu \) fraction of the cloud parcel with \( (1 - \mu) \) fraction of the second (sub-saturated) parcel. The mixing cloud fraction may vary within the range of \( 0 \leq \mu \leq 1 \). Therefore, the mass of the resulting mixed parcel is equal to \( m_1\mu + (1 - \mu)m_2 = 1 \). This approach simplifies the consideration of mixing and allows considering all possible proportions of the mixing of two volumes.
2.3 Effect of mixing on liquid water and temperature

The mixing ratio of liquid water \( q \) formed at the final stage of mixing is determined by the mass of the mixing cloud water \( \mu q_1 \) and amount of evaporated water required to saturate the newly formed mixed volume \( \delta q_m \). The mass balance of liquid water for the mixing volume yields

\[
q = \mu q_1 - \delta q_m ,
\]

where

\[
\delta q_m = \frac{c_p R_v T_{m0}^2}{L^2} \ln \left( \frac{1 + \left( \frac{e_s(T_{m0}) R_v L}{p c_p R_v^2 T_{m0}^2} \right)}{1 + RH_{m0} \left( \frac{e_s(T_{m0}) R_v L}{p c_p R_v^2 T_{m0}^2} \right)} \right) \approx \frac{S_{m0}}{A_2} \tag{2}
\]

is the mixing ratio of liquid water required to saturate 1kg of volume with temperature \( T_{m0} \) and humidity \( RH_{m0} \) (appendix A); \( T_{m0}, RH_{m0} \) and \( S_{m0} \), are the temperature, relative humidity formed and supersaturation formed in the volume after instantaneous air mixing, but before droplets start evaporating (appendix A); \( e_s(T_{m0}) \) is saturation vapor pressure at temperature \( T_{m0} \).

Eq. (1) is a non-linear function of \( \mu \), since \( T_{m0}, e_{m0} \) and thus \( \delta q_m \) depend on \( \mu \). Eq.(1) can be simplified, if \( T_1 = T_2 \). In this case \( T_{m0} = T_1 = T_2 \), and \( e_s(T_{m0}) = e_s(T_1) = e_s(T_2) \). Given that, the expression under logarithm in Eq.(2) can be expanded in series resulting in (appendix B)

\[
\delta q_m = (1 - \mu) \delta q^* , \tag{3}
\]

where

\[
\delta q^* = \frac{c_p R_v T_2^2}{L^2} \ln \left( \frac{1 + \left( \frac{e_s(T_2) R_v L}{p c_p R_v^2 T_2^2} \right)}{1 + RH_2 \left( \frac{e_s(T_2) R_v L}{p c_p R_v^2 T_2^2} \right)} \right) \approx \frac{S_2}{A_2} \tag{4}
\]

is the mixing ratio of liquid water required to saturate 1 kg of the entrained dry air. Substituting Eq.(3) in Eq.(1) gives

\[
q = \mu q_1 - (1 - \mu) \delta q^* , \tag{5}
\]

The value of \( \delta q^* \) does not depend on \( \mu \), and Eq. (5) is a simple linear function of \( \mu \). The comparisons with numerical simulations showed, that Eq.(5) provides accuracy within few percent, when the temperature difference \( |T_1 - T_2| < 2^\circ \text{C} \). Although, in many cases \( |T_1 - T_2| \) may vary a wide range reaching \( 10^\circ \text{C} \) or higher, clouds with \( |T_1 - T_2| < 2^\circ \text{C} \) are quite common. Therefore, for
the sake of simplicity, Eq.(5) and the assumption $T_1 \approx T_2$ will be used in the following consideration of mixing.

It should be noted that, Eqs (1) and (5) are valid for the cases, when $\mu > \mu_{cr}$. Here $\mu_{cr}$ is critical mixing fraction, which separates partial and complete evaporation of cloud water in the mixing volume (section 2.4). Cases when $\mu \leq \mu_{cr}$ correspond to complete evaporation of droplets, and $q = 0$.

The temperature at the final stage of mixing can be estimated as (appendix C)

$$T = T_{m0} - \frac{(1 - \mu) \delta q^* L}{c_{pu}}, \quad \text{when } \mu > \mu_{cr} \quad (6a)$$

$$T = T_{m0} - \frac{\mu q_1 L}{c_{pu}}, \quad \text{when } \mu \leq \mu_{cr} \quad (6b)$$

Eqs. (1), (5), (6) were obtained based on mass and energy conservation, and they do not depend on how mixing proceeds. Therefore, Eqs. (1), (5), (6) are valid for both homogeneous and inhomogeneous mixing.

2.4 Complete evaporation

As mentioned in section 2.2 the process of mixing is complete only after reaching equilibrium by saturating the mixed volume or by evaporating of all cloud droplets depending on the mixing fraction $\mu$. The critical mixing fraction $\mu_{cr}$, corresponding to evaporation of all droplets, can be found from Eq.(5) when $q = 0$, i.e.

$$\mu_{cr} = - \frac{\delta q^*}{q_1 + \delta q^*} \quad (7)$$

Critical mixing fraction separates $\mu$ in two subranges: (a) $1 \geq \mu > \mu_{cr}$ where $q$ is described by Eqs.(1) or (5) and $RH_m = 1$; (b) $\mu_{cr} \geq \mu \geq 0$ where $q = 0$ and $RH_m \leq 1$.

For the general case when $T_1 \neq T_2$, $\mu_{cr}$, can be found by solving the non-linear equation

$$\mu_{cr} q_1 - \delta q_m(\mu_{cr}) = 0 \quad (8)$$

Figure 2 shows comparisons of dependences of $\mu_{cr}$ vs. $q_1$ calculated from Eq. (7) and those deduced from a numerical model (Sect. 3). Critical mixing fraction $\mu_{cr}$ is also shown by black stars in Fig. 4. The locations of the stars in Fig.4 coincide well with the locations, where the modeled
microphysical moments become zero. The obtained agreement between analytical and modeled \( \mu_{cr} \) in Figs. 2 and 4 validates the developed approach.

### 2.5 Extreme inhomogeneous mixing

Within the framework of **extreme inhomogeneous** mixing some fraction of droplets undergo complete evaporation, whereas the rest of the droplets remain unchanged. Therefore, such a process results in scaling the droplet size distribution \( f(D) \), i.e.

\[
f(D) = kf_1(D)
\]

where \( k \) is some coefficient dependent on \( \mu \) and the initial environmental parameters of the mixing volumes, \( f_1(D) \) is the droplet size distribution before mixing. Equation (9) yields relationships between pairs \( n \)-th and \( k \)-th moments

\[
\frac{M_n}{M_{n1}} = \frac{M_k}{M_{k1}}
\]

where \( M_n = \int_0^\infty f(D)D^n dD \) is the \( n \)-th moment of \( f(D) \). Therefore, it is anticipated that for **extreme inhomogeneous** mixing droplet number concentration \( N \) (0th moment), extinction coefficient \( \beta \) (2nd moment), liquid water mixing ratio \( q \) (3rd moment), along with other moments, will correlate with each other, i.e.

\[
\frac{N}{N_1} = \frac{\beta}{\beta_1} = \frac{q}{q_1}
\]

One of the consequences of Eqs. (9)-(11) is that the characteristic droplet sizes \( \overline{D}, D_2, D_v, D_{eff} \) will remain constant during inhomogeneous mixing.

For the case \( T_1 = T_2 \) and \( \mu > \mu_{cr} \) Eqs. (5) and (11) yield the dependence of \( N \) vs. \( \mu \)

\[
N = N_1 \left( \mu - \frac{(1 - \mu)\delta q^*}{q_1} \right)
\]

\[
\beta = \beta_1 \left( \mu - \frac{(1 - \mu)\delta q^*}{q_1} \right)
\]

For a general case when \( T_1 \neq T_2 \) the term \( (1 - \mu)\delta q^* \) in Eqs. (12) and (13) should be replaced by \( \delta q_m(\mu) \) (Eq.(2)).
### 2.6 Homogeneous mixing

For homogeneous mixing, when \( \mu > \mu_{cr} \), the droplet number concentration changes only due to dilution by the entrained air, i.e.

\[
\frac{N}{N_1} = \mu
\]

(14)

Assuming \( T_1 = T_2 \), and substituting Eq. (5) in (14) yields:

\[
\frac{N}{N_1} = \frac{q + \delta q^*}{q_l + \delta q^*}
\]

(15)

As follows from Eq. (15) \( N \) and \( q \) are linearly related for homogeneous mixing. However, no linear relationships exist between other moments. Thus, substituting the definition of the liquid water mixing ratio \( q = \pi \rho_w N D_v^3 / 6 \rho_a \) in Eq. (15) yields the relationship between mean volume droplet size and concentration

\[
\frac{D_v^3}{D_{v1}^3} = 1 + \left( 1 - \frac{N_0}{N} \right) \frac{\delta q^*}{q_l}
\]

(16a)

\[
\frac{D_v^3}{D_{v1}^3} = q \left( \frac{q_l + \delta q^*}{q + \delta q^*} \right)
\]

(16b)

In a similar way the relationship between the extinction coefficient \( \beta = Q \pi N D_v^2 / 4 \), \( N \) and \( q \) can be written as

\[
\frac{\beta}{\beta_l} = \frac{N}{N_1} \left( 1 + \left( 1 - \frac{N_0}{N} \right) \frac{\delta q^*}{q_l} \right)^{2/3}
\]

(17a)

\[
\frac{\beta}{\beta_l} = \left( \frac{q}{q_l} \right)^{2/3} \left( \frac{q + \delta q^*}{q_l + \delta q^*} \right)^{2/3}
\]

(17b)

In Eqs. (17a) and (17b) it is assumed that \( D_v \approx D_v \).

Substituting in Eq. (16) the expression for the time of phase relaxation \( \tau_p = 1/b N \bar{D} \) (e.g. Squires 1953; Korolev and Mazin, 2003) and assuming \( \bar{D} \approx D_v \) yields

\[
\frac{\tau}{\tau_l} = \frac{N}{N_1} \left( 1 + \left( 1 - \frac{N_0}{N} \right) \frac{\delta q^*}{q_l} \right)^{-1/3}
\]

(18)

For the cases when the temperature difference \( |T_1 - T_2| \) exceeds a few degrees, the effect of \( \mu \) on \( T_m \) and \( S_m \) should be taken into consideration in the calculations of evaporated water. For such
cases $\delta q_m$ (Eq. (2)) should be used instead of $\delta q^*$. Using Eq. (14) $\delta q_m$ can be presented as a function of $\frac{N}{N_1}$, i.e. $\delta q_m(\mu) = \delta q_m\left(\frac{N}{N_1}\right)$. Replacing Eq. (5) by (1) in the above consideration, the equations Eqs. (15)-(18) can be rewritten as

$$\frac{N}{N_1} = q + \delta q_m\left(\frac{N}{N_1}\right)$$  \hspace{1cm} (19)$$

$$\frac{D_{v^3}}{D_{v^3c}} = 1 - \frac{\delta q_m\left(\frac{N}{N_1}\right)}{q} = \frac{q + \delta q_m\left(\frac{q}{q_1}\right)}{q_1}$$  \hspace{1cm} (20)$$

$$\beta = \frac{N}{N_1} \left(1 - \frac{\delta q_m\left(\frac{N}{N_1}\right)}{q} \right)^{\frac{1}{2\mu}} = \frac{q^{1/2} \left(q + \delta q_m\left(\frac{\beta}{\beta_1}\right)\right)^{1/2}}{q_1}$$  \hspace{1cm} (21)$$

$$\tau_p = \frac{N_1}{N} \left(1 - \frac{\delta q_m\left(\frac{N}{N_0}\right)N_1}{q_1}\right)^{\frac{1}{2}}$$  \hspace{1cm} (22)$$

Eqs. (19)-(22) can be solved numerically.

### 2.7 Degenerate case

As follows from Eq.(5), if

$$\frac{(1 - \mu)}{\mu} \frac{\delta q^*}{q_1} \ll 1$$  \hspace{1cm} (23)$$

then $q_1 \geq q \gg \delta q^*$. If the condition in Eq. (23) is valid, then the terms associated with $\delta q^*$ in Eqs. (15)-(18) can be neglected. This results in correlation of all moments, i.e. $N/N_1 = \beta/\beta_1 = q/q_1$ (compare with Eq.(11)). This corresponds to the degenerate case, when the difference between the homogeneous and inhomogeneous mixing vanishes. Thus, the dimensionless parameter $\xi = \frac{1 - \mu}{\mu} \frac{\delta q^*}{q_1}$ can be used for characterization of proximity of the homogeneous mixing moments to those formed during extremely inhomogeneous mixing.
The range of $\mu$ in $\xi$ is limited by $\mu_{cr} < \mu \leq 1$, so that $0 < \frac{1-\mu}{\mu} \leq \frac{q_1}{\delta q^*}$. This gives the range of changes of $\xi$, i.e. $0 \leq \xi \leq 1$ for the mixing without complete evaporation of droplets. The degenerate case corresponds to $\xi \to 0$, whereas $\xi \to 1$ corresponds to maximum difference of the moments for homogeneous and extremely inhomogeneous mixing.

As follows from Eqs. (4) and (23) approaching to the degenerate case ($\xi \to 0$) occurs, when one of the following conditions or their combination is satisfied: (a) $R_H^2 \to 1$; (b) $E_s(T) \to 0$ at low temperatures; (c) $q_1 \gg \delta q^*$; (d) $\mu \to 1$. The effect of $R_H$, $T$, $q_1$ and $\mu$ on mixing will be demonstrated in Sect.3.

Figure 3 shows dependence of $\xi$ vs. $\mu$. The grey area in Fig.3 indicates the region where identification of type of mixing from in-situ measurements (Sect.5) may be hindered due to proximity of the moments for homogeneous and inhomogeneous mixing. Thus for $\delta q^*/q_1 \approx 0.01$ identification of type of mixing is ambiguous for nearly the entire range of $\mu$.

For the general case, when $T_1 \neq T_2$, it should be $\xi = \frac{|\delta q_m(\mu)|}{\mu q_1}$. An absolute value $|\delta q_m(\mu)|$ should be used in $\xi$ since $\delta q_m(\mu)$ can be negative (Appendix A, Fig.A1) if mixing results in supersaturation Sect. 3.4).

The coefficient $\xi$ may be useful for identification type of mixing from in-situ observations. It is worth noting, that the ratio $\frac{\delta q^*}{q_1} \approx \frac{S_2}{A_2 q_1}$ is equal to the parameter $R$ (Pinsky et al. 2015ab), which plays an important role in determining scenarios of droplet evaporation in turbulent environment.

3 Comparisons with numerical simulations

Numerical simulations were performed to examine accuracy and limitations of the analytical expressions in Sect.2 and to conduct a sensitivity test to environmental and cloud parameters. The simulations have been performed with the help of a parcel model similar to that in Korolev (1995). The ensemble of droplets in the simulation was assumed to be monodisperse. For the case of extreme inhomogeneous mixing the amount of evaporated water $\Delta q$ required to saturate the mixed volume was calculated first. If $\Delta q < \mu q_1$, then the concentration of evaporated droplets was calculated as $N_{ev} = \frac{\Delta q}{m_d \rho_a}$, where $m_d = \pi \rho_w D^3/6$. Then, the concentration of the remaining droplets $N = N_1 - N_{ev}$ was recalculated based on the calculation on the volume formed after mixing. If $\Delta q \geq \mu q_1$, then all droplets evaporate, and $N = 0$. 
For the case of homogeneous mixing in the first step the engulfed parcel instantly mixes with the cloud parcel resulting in a new humidity $RH_{m0}$, temperature $T_{m0}$ and volume $V_{m0}$. After that the droplets start evaporating until either their complete evaporation or saturation over liquid is reached. The calculations stopped when, either $D < 0.2\mu m$ or $(E_s - e)/E_s < 0.001$, respectively.

3.1 Effect of mixing fraction

Figure 4 shows the results of the simulation of different moments and state parameters vs. $\mu$. The calculations were performed for different relative humidity of the entrained parcel $RH_2 = 0.2$, 0.5, 0.8 and 0.95. As seen from Fig.4 for the case of homogeneous mixing only $N$ and $q$ are linearly related with $\mu$, the rest of the variables have non-linear dependences on $\mu$. For the case of inhomogeneous mixing all $f(D)$ moments and droplet sizes linearly depend on $\mu$. Note, for $\mu \leq \mu_{cr}$ all moments are equal to zero.

Since the amount of the evaporated liquid water does not depend on the type of mixing, the dependences of $q(\mu)$ are the same for both homogeneous and inhomogeneous mixing (Fig.4a). The type of mixing has the most pronounced effect on the droplet concentration (Fig.4b) and droplet sizes (Fig.4e).

Figure 4g shows the dependences $RH_{m0}$ and $RH$ vs. $\mu$, Here $RH_{m0}$ is the relative humidity at the initial stage of homogeneous mixing before droplets start evaporating (Fig. 1b2). Figure 3h presents comparisons of modeled $T(\mu)$ and those calculated from Eqs.(6a,b) and (C4). The independence of $q(\mu)$, $RH(\mu)$ and $T(\mu)$ on type of mixing (Fig.4a,g,h) is the consequence of the mass and energy conservation, which are not contingent on type of mixing.

3.2 Effect of humidity of entrained air

The diagrams in Fig. 5a-c show the dependences of normalized $\beta$, $q$ and $D_{\nu}$ vs. $N/N_0$ calculated from numerical simulations and analytical equations from Sect. 2. The calculations were performed for different humidity of the entrained air $RH_2$. As seen from Fig. 5a-c, the normalized dependences for homogeneous mixing $q(N)$, $\beta(N)$ and $D_{\nu}(N)$ tend to approach the line of extreme inhomogeneous mixing when relative humidity $RH_2$ approaches to 1. This is consistent with the degenerate case, when $\xi \rightarrow 0$ (Sect.2.7). In this case droplets behave as a passive admixture, and they do not interact with the environment.
3.3 Effect of liquid water mixing ratio

Figure 5d-f demonstrate the sensitivity of \( q(N), \beta(N) \) and \( D_v(N) \) to liquid water mixing ratio \( q_1 \). It is seen, that the increase of \( q_1 \) results in \( q(N), \beta(N) \) and \( D_v(N) \) (calculated for homogeneous mixing) approaching towards \( q(N), \beta(N) \) and \( D_v(N) \) for the inhomogeneous mixing. In other words, the sensitivity of the microphysical parameters to the type of mixing increases with the decrease of \( q_1 \). From a practical viewpoint it means, that from in-situ observations the difference between homogeneous and inhomogeneous mixing is anticipated to be more pronounced for the cases with a relatively low liquid water mixing ratio (e.g. \( q_1 < 1 \text{g/kg} \)). Such behaviour is consistent with the consideration in Sect. 2.7.

3.4 Effect of temperature \( T_1 = T_2 \)

Figure 5g-j shows the effect of temperature on the normalized \( q(N), \beta(N) \) and \( D_v(N) \) for \( T_1 = T_2 \). Figure 5g-j indicate that the difference between the moments becomes most pronounced at warm temperatures, whereas at cold temperatures (e.g. \( T= -30^\circ\text{C} \)), \( q(N), \beta(N) \) and \( D_v(N) \) for homogeneous mixing are approaching those for the extreme inhomogeneous mixing limit.

Such behavior is explained by the fact that liquid water deficit \( \delta q_m \) decreases with decreasing temperature (appendix A, Fig. A1). At low temperatures (\( T= -30^\circ\text{C} \)) the amount of evaporated water \( \delta q_m \) is so small, that homogeneous mixing with dry out-of-cloud air will have approximately the same effect as mixing with saturated air (i.e. degenerate case, Sect. 2.7).

Overall, as follows from Fig.5 the results the analytical predictions (Sect. 2) turned out to be in a good agreement with numerical simulations.

3.5 Effect of temperature \( T_1 \neq T_2 \)

Isobaric mixing of two nearly saturated volumes with \( T_1 \neq T_2 \) may result in supersaturated environment (e.g. Rogers, 1976; Bohren and Albrecht, 1998). Mixing resulting in supersaturation is different in principle from the mixing with evaporating droplets. In this case the meaning of homogeneous and inhomogeneous mixing becomes ambiguous. Formation of supersaturation leads to different dependences between \( N\bar{D}, \beta, q, \bar{D} \) and \( N \) as compared to those shown in Figs. 3–4, when \( T_1 = T_2 \).

Figure 6 presents a set of diagrams similar to those in Fig.4, but calculated for the cases when \( T_1 \leq T_2 \). It turns out that for the case of extreme inhomogeneous mixing the temperature difference
between $T_1$ and $T_2$ breaks down linear dependences of the microphysical moments (e.g. $N\bar{D}$, $\beta$, $q$
Fig. 6a,c,d) vs. $\mu$.

Figure 7 presents the effect of the temperature difference $\Delta T$ on the normalized dependences
$q(N)$, $\beta(N)$ and $D_v(N)$. In clouds, high supersaturation resulting from isobaric mixing may lead to
activation of interstitial CCN, which may increase $N$ and decrease $D_v$ (Korolev and Isaac, 2000).
However, no activation of new droplets during isobaric mixing was allowed in this study. For the
cases when $RH_{m0} > 1$ (Fig. 7, AB on line 1) the condensed water was uniformly distributed
between available droplets. Therefore, $q(N)$, $\beta(N)$ and $D_v(N)$ calculated for homogeneous and
extremely inhomogeneous mixing coincide with each other on this interval.

Numerical simulations also showed, that the effect of temperature on mixing is more
pronounced for the cases when the cloud temperature is warmer than that of the entrained air, i.e.
$T_1 > T_2$, as compared to the cases with $T_1 < T_2$.

4. Progressive mixing

4.1 Effect on microphysical parameters

In the previous sections the mixing was considered as a single event, i.e. $\mu$ fraction of the cloudy
air mixed up with $(1 - \mu)$ fraction of entrained dry air. Such mixing will be referred to as “primary”
mixing. Primary mixing results in an ensemble of elementary volumes characterized by a set of
microphysical and state parameters i.e. $\bar{D}(\mu)$, $N(\mu)$, $RH(\mu)$, $T(\mu)$, etc. Each of these parameters
has a functional dependence on $\mu$, and what is important, these parameters have functional
relationships between each other.

In reality mixing is a continuous process. It does not stop after the primary mixing. The
elementary volumes formed after primary mixing continue to progressively mix with each other.

The second stage of mixing will result in an ensemble of elementary volumes characterized by
a set of parameters $D_v^{(2)}$, $N^{(2)}$, $RH^{(2)}$, $T^{(2)}$, etc. Here the superscript $(2)$ indicates the stage of mixing.
After the second stage the mixed volumes undergo subsequent stages of mixing.

The idealised conceptual diagram of the progressive mixing is shown in Fig. 8. As mentioned
in Sect. 2.1, the actual process of mixing is indeed much more complex than the sequence of discrete
events portrayed in Fig.8. However, as it will be shown below, this simplified consideration of
allows establishing main features of evolution of relationships between the microphysical moments
affected by mixing. The obtained results facilitates identification of type of mixing from in-situ measurements.

Progressive mixing was simulated with the help of a numerical model, where parcels were randomly mixed with each other and with the cloud environment. The mixing fraction \( \mu \) was also set to be random during each mixing event. Models of stochastic mixing have been used in a number of studies (e.g. Krueger et al., 1997; Su et al., 1998; Burnet and Brenguier, 2007). In the present work the analysis of progressive mixing is expanded to examine its effect on the relationship between moments of the droplet size distribution.

The results of the progressive mixing for the first four stages are presented in Fig. 9. As seen from Fig. 9 the functional relationship between the pairs of microphysical and state parameters exists only for the primary stage. For higher mixing stages these functional relationships break down. Thus, cloud volumes with the same \( N^{(2)} \) may have different \( D_v^{(2)} \). Figure 9 also shows that the regions of scattering of \( q(N), \beta(N) \) and \( D_v(N) \) for stages 2, 3 and 4 are limited from above by the inhomogeneous mixing (red dashed lines) and from below by primary homogeneous mixing (red solid lines).

Figure 10 presents a conceptual \( N - q \) diagram explaining breaking the functional relationships during progressive homogeneous mixing. After the first stage of mixing the \( N - q \) points will be scattered along the line \( OB \) and point \( C \). The line \( OB \) corresponds to the ensemble of points with \( RH = 1 \). Therefore, result of mixing between two saturated volumes randomly selected on \( AB \), will remain on the same line. Point \( C \) corresponds to the ensemble of points with \( N = 0, RH_2 \leq RH_C( \mu^{(1)} ) \leq 1 \), where \( 0 \leq \mu^{(1)} < \mu_{cr} \). Therefore, mixing between point \( A \) (Fig.10) and point \( C \), when \( RH = 1 \) will result in scattering along the line \( AC \) (degenerate case). Points resulted from mixing between \( A \) (\( RH = 1 \)) and point \( C \), when \( RH_2 \leq RH_C < 1 \), will scattered over the ensemble of dashed lines shown in Fig.10. These lines will fill the sector \( CAB \). Random mixing between points on the line \( OB \) and \( C \), will eventually fill the entire sector \( COB \). The same consideration can be applied to progressive mixing between other moments.

During the progressive mixing \( N^{(n)}, \beta^{(n)}, q^{(n)} \) and \( D_v^{(n)} \) formed in the elementary parcels tend to approach those in the undiluted cloud, i.e. \( N_1, \beta_1, q_1 \) and \( D_{v1} \). This process can be considered as a surrogate to the diffusion process between the cloud and sub-saturated out-of-cloud environment. The convergence of \( \beta^{(n)}, q^{(n)} \) and \( D_v^{(n)} \) during the progressive mixing can be seen in Fig. 9, where
the scattering of normalized $q^{(n)}(N)$, $\beta^{(n)}(N)$ and $D_v^{(n)}(N)$ becomes denser towards the top-right corner (1,1) with the increase of the stage of mixing.

It is worth noting that progressive mixing with the dry air does not break the functional relationships between the moments. This case is equivalent to detrainment of cloudy environment into dry air. It can be shown that Eq.(14) remain valid at any stage of progressive homogeneous mixing with dry air only, i.e. $N_j/N_1 = \mu^{(1)} \cdots \mu^{(j-1)} \mu^{(j)}$, where $\mu^{(j)}$ is the mixing fraction at the $j$-th stage of mixing. Eqs. (15)-(24) also remain valid for the progressive mixing with the dry air only.

As follows from Eq. (9) for the case of extreme inhomogeneous mixing the progressive mixing does not affect the functional relations between $N^{(n)}$, $\beta^{(n)}$, $q^{(n)}$ and $D_v^{(n)}$ and other microphysical parameters. These relations remain the same regardless of the actual stage of mixing. This is one of the fundamental differences between homogeneous and inhomogeneous mixing, which can be used for identification of type of mixing from in-situ measurements.

4.2 Effect on droplet size distributions

Figure 11 shows modeled droplet size distributions averaged over the ensembles of elementary volumes corresponding to the first four stages of homogeneous mixing. As seen from Fig. 11a–d for the case with $T_1 = T_2$ the droplet size distributions are broadened towards small sizes. Depending on the stage of mixing and mixing fraction $\mu$ the size distributions formed in each elementary volume may be unimodal or multimodal. However, due to the random nature of the modal sizes formed during mixing, the average size distributions become smooth and unimodal (Fig.11a-d).

Broadening of droplet size distributions towards small sizes during homogeneous mixing is well known and it was demonstrated in a number of studies (e.g. Baker and Latham, 1982; Jensen and Baker, 1989; Jeffery, 2007; Kumar et al., 2013). However, if mixing results in supersaturation (section 3.4), then the droplet size distribution may broaden towards larger sizes (Fig. 11e–h). For this to occur, both the temperature difference between the cloud and the environment $|T_1 - T_2|$ and the relative humidity of the environment $RH_2$ must be sufficiently large. Such conditions are inherently unstable, however, this might occur in regions that have been moistened through prior cloud detrainment. Thus homogeneous mixing may result in broadening of droplet size distributions towards either smaller or larger sizes (Fig.11).
These results were obtained in the frame of the formalism of homogeneous and inhomogeneous mixing. The following two works in this series (Pinsky et al., 2016a, b) will discuss the broadening of polydisperse and monodisperse $f(D)$ during both homogeneous and inhomogeneous mixing in greater details.

5 Identification of type of mixing from in-situ observations

The purpose of this section is to attempt identifying type of mixing based on examining relationships between basic microphysical parameters $N$, $\beta$, $LWC$, $D_v$ measured from in-situ.

5.1 Expected relationships between the moments

Prior proceeding with the analysis of in-situ data we summarize the results of the previous consideration on how homogeneous and extreme inhomogeneous mixing is expected to manifest itself in relationships between basic microphysical parameters, such as $N$, $\beta$, $q$ and $D_v$.

For extreme inhomogeneous mixing the relationship between the pairs of $N$, $\beta$ and $q$ are determined by linear dependences $M_n = \alpha_{nk}M_k$ (Eq. 10) at any stage of mixing. As follows from Eq. (11) the slopes $\alpha_{nk}$ for $q(N)$, $\beta(N)$ and $q(\beta)$ are equal to the ratios $q_1/N_1$, $\beta_1/N_1$, and $q_1/\beta_1$, respectively, where $N_1$, $\beta_1$ and $q_1$ correspond to undiluted adiabatic values. The values of $N_1$, $\beta_1$ and $q_1$ may vary depending on the location inside the cloud and environmental conditions at the cloud base. Thus, the adiabatic value of $q_1$ is a function of elevation above the cloud base $\Delta Z$, whereas $N_1$ depends on the vertical velocity at the cloud base $u_z$ and the aerosol load. Therefore, the scattering of $q - N$ points will be aligned along an ensemble of different lines determined by $q_1/N_1$, which are specific to different cloud volumes. The conceptual diagram of the scattering of $q - N$ measurements in a cloud with extreme inhomogeneous mixing is shown in Fig. 12a. The scatter diagrams for other moments (e.g. $q - \beta$, $N - \beta$) will have the similar patterns as that in Fig. 12a.

For the case of homogeneous mixing the functional relationship between the pairs of $N$, $\beta$, $q$ and $D_v$ are disrupted by a progressive mixing. As shown in Sect. 4.1 the ensemble of points of $N$, $\beta$ and $q$ will be scattered within a sector, which is limited by lines determined by Eq. (11) (extreme inhomogeneous mixing) and Eqs. (15)-(17) (primary homogeneous), respectively (Fig. 9). What is important, is that the top of the sectors for $q(N)$ and $\beta(N)$ correspond to points $[N_1, q_1]$ and $[N_1, \beta_1]$, respectively. Since $N_1$, $\beta_1$ and $q_1$ may vary within the same cloud, it is anticipated that the $N$, $\beta$ and $q$ measurements will be scattered within an ensemble of sectors as shown in Fig. 12b.
It is important to note that during homogeneous mixing prior reaching equilibrium, functional relationships between the microphysical moments do not exist either. After the instant mixing of cloud fraction $\mu$ with entrained air (Fig. 1b(2)), $q_{m0} = \mu q_0$ and $N_{m0} = \mu N_0$. This state corresponds to point $D$ in Fig.10. After that droplets start evaporating until liquid mixing ratio reaches point $A$ (Fig.10), which corresponds to the equilibrium state ($RH = 1$). Therefore, during evaporation time $q - N$ points will be scattered along the line $AD$. Since, point $D$ can be located anywhere on $OC$, the ensemble of $q - N$ points corresponding to non-equilibrium state will fill the $COB$ area.

Thus, the absence of the functional relationships between the moments during homogeneous mixing may occur both during progressive mixing and during primary mixing prior reaching the equilibrium state. The evaporation time required to reach equilibrium during homogeneous mixing is discussed in details in Pinsky et al. (2016b), and it is usually limited by few tens of seconds. However, progressive mixing is not limited in time. Therefore, it is very likely that no functional relationship between microphysical parameters will be observed during in-situ measurements.

Fig.12 demonstrated a fundamental difference in scattering of $q - N$ for homogeneous and [extreme inhomogeneous](#) mixing, which will be used to facilitate identification of type of mixing in the following section.

### 5.2 Results of observations

The measurements were obtained on the University of Wyoming King Air aircraft during the COPE-MED project in South-Western part of UK during July-August 2013 (Leon et al., 2016). The UW King Air was equipped with a suite of microphysical instruments, including a DMT Cloud Droplet probe (CDP), designed for measurements of droplet sizes and their concentrations in the nominal size ranges $1–50 \mu m$.

Figure 13 shows a time series of droplet concentration, extinction coefficient, liquid water content and mean volume droplet diameter measured by the CDP during transit through a convective cell on 18 July 2013. The CDP data were sampled at 10Hz, which corresponds to approximately 10m spatial averaging. Visual examination of the spatial changes of $N$, $\beta$ and $LWC$ shows strong correlation. The amplitude of changes of these parameters reaches nearly one hundred percent with respect to their maximum. Contrary to that, the spatial variations of $\bar{D}$ and $D_v$ are quite conservative and their values remain nearly constant. With the exception of two cloud holes
between 13:50:42 and 13:50:44, the amplitude of fluctuations of $D_v$ does not exceed 8% with standard deviation of 2.2%.

Figure 14 shows scatter diagrams of $LWC(N)$, $\beta(N)$, $LWC(\beta)$ and $D_v(N)$ measured by the CDP during seven consecutive penetrations of the same convective cell extended over a period of approximately 19 min. One of these penetrations is shown in Fig. 13. The measurements were conducted at $H = 5500m$ and $T = -12^\circ C$. The relative humidity of the ambient air was approximately 20%. At the beginning of the sampling no precipitation size particles were observed in the cloud. However, by the end of the sampling period some raindrops and ice crystals were present in the cloud. Despite the presence of some precipitation size particles, the scatter diagrams in Fig. 14a, b and d demonstrate high correlation between pairs $N$, $\beta$ and $LWC$. The mean volume diameter in Fig. 14c shows very little changes from 19 to 17 μm when concentration changes from 1100 to 500 cm$^{-3}$, However, for $N < 200$ cm$^{-3}$, the volume diameter decreases to 12–15 μm.

Red lines in Fig. 14 indicate $q(N)$, $\beta(N)$, $LWC(\beta)$ and $D_v(N)$ calculated for the 1st stage of homogeneous mixing. The calculations were performed for a monodisperse $f(D)$ with $D_1=18.5\mu m$, $N_1 = 1100$ cm$^{-3}$, and state parameters as during the measurements. Comparisons of dependences $q(N)$, $\beta(N)$, $LWC(\beta)$ and $D_v(N)$ based on in-situ measurements with those obtained from numerical simulations of homogeneous mixing show minor difference for high concentrations 700 cm$^{-3} < N < 1100$ cm$^{-3}$ (Fig. 14a–c). Simulation also shows that for this specific case the difference between homogeneous and inhomogeneous mixing does not exceed 10% when $700$ cm$^{-3} < N < 1100$ cm$^{-3}$. Such difference remains within the errors of measurements. Therefore, in this specific cloud for the regions with $N > 700$ cm$^{-3}$ the type of mixing cannot be unambiguously identified from the analysis of the dependences $LWC(N)$, $\beta(N)$, $LWC(\beta)$ and $D_v(N)$. This is consistent with the assessment of feasibility of segregation of homogeneous and inhomogeneous mixing in Fig.3 (dashed line). Since for homogeneous mixing $N \propto \mu$, than Fig.3 suggests good separation of the moments for $N > 700$ cm$^{-3}$.

For the regions with $N < 500$ cm$^{-3}$ the deviation between homogeneous mixing simulations and in-situ measurements in Fig.14 becomes well pronounced and it extends beyond possible errors of measurements. This suggests that the mixing is in these regions is dominated by the extreme inhomogeneous type.

Figure 15 shows the same type of diagrams as in Fig. 14, which were measured during 45 consecutive traverses through an ensemble of deep convective cells. The sampling altitude varied
in the range $3000 \text{m} < H < 4500 \text{m}$, temperature $-11^\circ \text{C} < T < 0^\circ \text{C}$, relative humidity in the vicinity of clouds $15\% < \text{RH} < 65\%$. The cloud measurements were extended over a period of $2 \text{h} 13 \text{m}$, which is suggestive that the convective cells were sampled at different stages of their lifetime. At the sampling level the concentration of raindrops varied from zero to few per liter, and their diameter did not exceed 2mm.

What is interesting that the scattering of the measurements $LWC(N), \beta(N)$ and $LWC(\beta)$ (Fig. 15a, b and d) is limited by the sector, which originates from the zero point as in Fig.12a. Analysis of the measurements showed that the data points $LWC(N), \beta(N), LWC(\beta)$ in each individual cloud traverse are well aligned along the lines with different slopes (e.g. Fig.14). After averaging over the ensemble of clouds, the area of the scattered points turned out to be located inside a sector limited by the lines with smallest and largest slopes.

Comparisons of the scatterdiagrams $LWC(N), \beta(N)$ and $LWC(\beta)$ in Figs.14 and 15 with the conceptual diagrams in Fig.12 unambiguously suggest that interaction between cloud and environment in the studied clouds was dominated by inhomogeneous mixing. It should be emphasized that analysis of a stand alone mixing diagram $N - D_\nu$ would not allow unambiguously draw such conclusion.

6. Discussion

One of the assumptions in most past studies is that for a sequence of the cloud samples collected along the flight path, the adiabatic values of $N_1, q_1, \beta_1, D_1$ and environmental parameters $e_2$ and $T_2$ remain the same. In fact these parameters may vary both within the same cloud or sequence of samples clouds, and the amplitude of their variations depends on microphysical and thermodynamical properties inside and outside the cloud environment. This variation will result in an ensemble of relationships $M_n = F_{nk}(M_k)$, and enhance scattering of the data points. In such cases identification of the type of mixing based on the $N - D_\nu$ diagram may result in confusion between homogeneous and inhomogeneous mixing. As demonstrated in Sect. 5, consideration of $N - q$ and $N - \beta$ diagrams may provide a better identification type of mixing.

Strictly speaking the identification of type of mixing from particle probe measurements as it was performed in Sect. 5 is incomplete. It allows establishing correlation between microphysical moments and makes a formal conclusion about the mixing type, however it does not allow judgement about stage of mixing (i.e. whether mixing is complete by reaching equilibrium). In most
previous studies, including this one, identification of type of mixing was based on the assumption that the sampled cloud volume is in equilibrium state \((RH = 1)\), and that it reached the final stage of mixing (Fig.1 a2, a3, b3). It is possible that at the moment of measurement the process of mixing is not complete and the droplet free filaments remained undersaturated (Fig.1 a1, b1, b2). In this case the relationship between different moments may be well described as \(M_n = \alpha_{nk}M_{nk}\) and the mixing be confused with inhomogeneous mixing.

In order to identify stage of mixing, high frequency collocated measurements of temperature and humidity are required. Unfortunately current technology does not allow such measurements yet.

Identification of type of mixing from in-situ observations is based on examination of relationships between moments of the size distributions measured along the flight path. The basic assumption underlying this analysis is that the cloud environment is not affected by other non-adiabatic processes.

Thus, collision-coalescence, riming or Wegener-Bergeron-Findeisen processes may change the droplet number concentration and liquid water content, and therefore, affect the relationship between the moments. Activation of interstitial CCN will result in breaking correlation between the moments due to formation of large concentration of droplets. Broad size distributions may also hinder identification of type of mixing due to partial evaporation of small droplets (Pinsky et al. 2016a).

It is anticipated that most suitable candidates to study mixing-entrainment process are non-precipitating convective clouds and stratocumulus clouds with relatively narrow droplet size distributions.

Another limiting factor is that the above consideration did not account for the effect of changing humidity in a vertically ascending parcel. Thus in droplet free entrained air relative humidity increases approximately 10% for \(\Delta z = 200m\) at \(T = 0 \, ^\circ C\). After reaching saturation the mixing turns into a degenerate case, which will appear as extreme inhomogeneous mixing. Joint effects of evaporating droplets and an increase in \(S\) during the vertical ascent may facilitate reaching saturation state. This case may also be relevant to the convective cloud described in Sect.5.2.
7. Conclusions

This study analyzes dependences of different moments of \( f(D) \) in the frame of formalism of homogeneous and extremely inhomogeneous mixing. The analysis was performed for the final stage of mixing based on the mass and energy conservation consideration. The following results were obtained in the frame of this study:

1. Simple analytical relationships between the main microphysical moments were obtained for the final state homogenous and extreme inhomogeneous mixing.

2. It was shown that the functional relationships between the moments exist only for the first stage of homogeneous mixing, when equilibrium is reached. Subsequent progressive homogeneous mixing breaks the functional relationship between the moments.

3. It was demonstrated that consideration of scattering \( N - LWC, N - \beta \) diagrams facilitates identification of type of mixing from in-situ measurements. For extreme inhomogeneous mixing the scattering of the data points \( N - LWC, N - \beta \) will be limited by a sector originating at zero point (Fig.12a). However, for homogeneous mixing the scattering data points will be limited by a sector originating at \( (N_1, LWC_1) \) and \( (N_1, \beta_1) \) (Fig.12b). Utilizing a stand-alone conventional \( N - D_v \) mixing diagram may not provide unambiguous answer about type of mixing.

4. The developed approach was applied to a set of in-situ measurements collected in convective clouds. The analysis of the dependences between \( N, \beta, LWC \) and \( D_v \) suggests that the interaction between entrained and cloudy environments for the studied clouds was dominated by inhomogeneous mixing.

The present study considers relationships between different moments of \( f(D) \) for the final stage of mixing. The following two works Pinsky et al. (2016a, b) in this series provide a detailed analysis of time dependences of droplet size distributions and its moments during homogeneous and inhomogeneous mixing.

Acknowledgement. The authors appreciate two anonymous reviewers for their comments. Alexei Korolev work was supported by Environment Canada and Transport Canada. The COPE-MED project was funded by National Science Foundation grant AGS-1230292 and AGS-1230203. The contribution of Mark Pinsky and Alex Khain was supported by the Israel Science Foundation (grant 1393/14), the Office of Science (BER), US Department of Energy Award DE-SC0006788 and the Binational US-Israel Science foundation (grant 2010446).
Appendix A: Liquid water deficit

The objective of this section is to find the amount of liquid water, which is required to be evaporated in order to saturate the parcel formed after mixing. Assume that $q_{v1}$, $q_{v2}$ are the mixing vapor ratios in the cloudy and entrained parcels, respectively, and $T_1$, $T_2$ are their respective initial temperatures. First, we find the saturation ratio $S_{m0}$ formed after instant mixing of the cloud and entrained before the cloud droplets start evaporating.

The vapor mixing ratio $q_{vm}$ formed in the mixed volume will be

$$q_{vm} = \mu q_{v1} + (1-\mu)q_{v2} \quad (A1)$$

The vapor pressure $e_m$ in the mixed volume can be derived from Eq. (A1) by substituting

$$e_m = p \frac{\mu + e_2 (p-e_1)}{p (e_1 - e_2)} \quad (A2)$$

The temperature of the mixed volume $T_{m0}$ can be found from the energy conservation law

$$\mu(q_v c_{pv} + c_{pa})(T_1 - T_{m0}) = (1-\mu)(q_{v2} c_{pv} + c_{pa})(T_{m0} - T_2) \quad (A3)$$

here $c_{pv}$, $c_{pa}$, are the specific heat capacitance of water vapor and dry air at constant pressure, respectively, $T_1$, $T_2$ are the initial temperatures in the first and second parcels before mixing. Substituting $q_{v1}$, $q_{v2}$ yields the temperature in the mixed volume

$$T_{m0} = \frac{\mu T_1 + \alpha (1-\mu)T_2}{\mu + \alpha (1-\mu)} \quad (A4)$$

where

$$\alpha = \frac{1 + \frac{c_{pv} R_v e_2}{c_{pa} R_e (p-e_2)}}{1 + \frac{c_{pv} R_v e_1}{c_{pa} R_e (p-e_1)}} \quad (A5)$$

With a good accuracy $\alpha \approx 1$. The resulting relative humidity after mixing the two volumes will be
\[ RH_{m0} = \frac{e_{m0}}{e_s(T_{m0})} \tag{A6} \]

where \( e_s(T_{m0}) \) is the saturated vapor pressure at temperature \( T_{m0} \).

The process of evaporation is accompanied by changing humidity and temperature due to latent heat of vaporization. This process is described by the Eq. (C2) in Korolev and Mazin (2003). Assuming the process to be isobaric (i.e. vertical velocity \( u_z = 0 \)) and absence of ice \( (dq_l = 0) \), Eq. (C2) (Korolev and Mazin, 2003) yields

\[ \frac{dS}{S+1} = \left( \frac{1}{S+1} \frac{pR_s}{e_s R_a} + \frac{L^2}{c_p R_i T^2} \right) dq \tag{A7} \]

Integrating Eq. (A7) from initial \( S_{m0} \) to saturation state, when \( S = 0 \), and taking into account that \( RH = S + 1 \), gives

\[ \delta q_m = -b \ln \left( \frac{1 + arH_{m0}}{1 + a} \right) \tag{A8} \]

the mixing ratio of liquid water required to evaporate in order to saturate 1kg of the cloud volume formed after mixing with the entrained air, but before droplet start evaporating. Here \( a = \frac{E_S R_a L^2}{p c_p R_i T_{m0}^2} \)

\[ b = \frac{c_p R_i T_{m0}^2}{L^2} \]

Since \( \left| \frac{A(RH_{m0} - 1)}{1 + A} \right| < 1 \), Eq.(A8) can be simplified as

\[ \delta q_m = ab \frac{1 - RH_{m0}}{1 + a} = - \frac{S_{m0}}{A_2} \tag{A9} \]

where \( A_2 = \frac{ab}{1+a} \). The analysis of Eqs. (A8)-(9) shows that for wide range of temperatures \(-30 \text{ °C} < T < 30 \text{ °C} \), both equations hold with high accuracy as long as the temperatures of the sub-saturated and cloud parcels \( |T_1 - T_2| < 10\text{°C} \).

Figure A1 shows comparisons of modeled \( \delta q_m \) and that calculated from Eqs. (A8) and (A9) for three different temperatures. The model solved a system of differential equation with incremental evaporation of liquid water until saturation is reached. As seen from Fig. A1 the agreement between modeled \( \delta q_m \) and that calculated from Eq. (A8)-(A9) is quite good and does not exceed few percent at \( RH_{m0} = 0.5 \). This discrepancy results from assumption that \( e_s \) and \( T \) are constant in Eqs.(A8)-(A9).
Appendix B: Liquid water deficit when $T_1 = T_2$

Eq.(A2) by assuming that $p \gg e_1$ and $p \gg e_2$ can be simplified as

$$e_{m0} = \mu e_1 + (1 - \mu)e_2$$  \hfill (B2)

As follows from Eq.(A4) for the case $T_1 = T_2$ with high accuracy $T_{m0} = T_1 = T_2$. Therefore,

$$e_S(T_{m0}) = e_S(T_1) = e_S(T_2).$$

Dividing Eq.(B1) by $e_S$ yields

$$RH_{m0} = \mu RH_1 + (1 - \mu)RH_2$$  \hfill (B3)

In most liquid clouds $RH_1 = 1$ (Korolev and Mazin 2003). Therefore, Eq.B2 turns into

$$RH_{m0} = \mu + (1 - \mu)RH_2$$  \hfill (B4)

Substituting Eq.(B4) in Eq.(B1) yields

$$\delta q_m = -b \ln \left(1 + \frac{a(1-\mu)(RH_2 - 1)}{1+a} \right)$$  \hfill (B5)

The expression under logarithm can be presented as the first two terms of the series expansion of $\left(1 + \frac{a(RH_2 - 1)}{1+a} \right)^{(1-\mu)}$. Substituting this expression into Eq.(B5), gives

$$\delta q_m = (1 - \mu)\delta q^*$$  \hfill (B6)

where

$$\delta q^* = -b \ln \left(1 + aRH_2 \right) \left(1 + a \right)$$  \hfill (B7)

is the mixing ratio of liquid water required to saturate 1 kg of the entrained dry volume.

Appendix C: Temperature in the mixing volume

The energy conservation for evaporating droplets can be written as

$$(T - T_{m0})(1 + q_{vm})c_{pm} + (1 - \mu)\delta q^* L = 0$$  \hfill (C1)

here $c_{pm}$ is the specific heat capacity of the moist air

$$c_{pm} = \frac{c_{pa} + q_{vm}c_{pv}}{1 + q_{vm}}$$  \hfill (C2)

Since $q_{vm} \ll 1$ and, $c_{pa} \approx c_{pm}$ Eq.(C1) may be simplified, so that the final temperature after mixing

$$T = T_{m0} - \frac{(1 - \mu)\delta q^* L}{c_{pa}}$$  \hfill (C3)
For the case when $T_1 \neq T_2$ Eq. (C3) should be replaced by

$$T = T_{m0} - \frac{\delta q_m L}{c_{pa}}$$  \hspace{1cm} (C4)$$

Eqs. (C3) and (C4) are valid for the mixing fraction $\mu > \mu_{cr}$. For $\mu \leq \mu_{cr}$ all entrained liquid water $\mu q_0$ evaporates, and the final temperature will be

$$T = T_{m0} - \frac{\mu q_0 L}{c_{pa}}$$  \hspace{1cm} (C5)$$

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58, 1998.
### Table 1

**List of Symbols**

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Description</th>
<th>Units</th>
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<tbody>
<tr>
<td>$A_2$</td>
<td>$\frac{p R_a + L^2}{e_s R_n c_p R_v T^2}$</td>
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</tr>
<tr>
<td>$a$</td>
<td>$\frac{e_s R_n L^2}{p c_p R_v^2 T^2}$</td>
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</tr>
<tr>
<td>$b$</td>
<td>$\frac{c_p R_v T^2}{L^2}$</td>
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<tr>
<td>$c_{pa}$</td>
<td>specific heat capacity of dry air at constant pressure</td>
<td>$J \ kg^{-1}K^{-1}$</td>
</tr>
<tr>
<td>$c_{pv}$</td>
<td>specific heat capacity of water vapor at constant pressure</td>
<td>$J \ kg^{-1}K^{-1}$</td>
</tr>
<tr>
<td>$\bar{D}$</td>
<td>mean droplet diameter</td>
<td>m</td>
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<tr>
<td>$D_2$</td>
<td>mean square droplet diameter</td>
<td>m</td>
</tr>
<tr>
<td>$D_v$</td>
<td>mean volume droplet diameter</td>
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<tr>
<td>$e$</td>
<td>water vapor pressure</td>
<td>N m$^{-2}$</td>
</tr>
<tr>
<td>$e_1$</td>
<td>initial water vapor pressure in the cloud parcel</td>
<td>N m$^{-2}$</td>
</tr>
<tr>
<td>$e_2$</td>
<td>initial water vapor pressure in the entrained sub-saturated parcel</td>
<td>N m$^{-2}$</td>
</tr>
<tr>
<td>$e_s$</td>
<td>saturation vapor pressure above flat surface of water</td>
<td>N m$^{-2}$</td>
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<tr>
<td>$f(D)$</td>
<td>size distribution of cloud droplets normalized on unity</td>
<td>m$^{-1}$</td>
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<tr>
<td>$L$</td>
<td>latent heat for liquid water</td>
<td>J kg$^{-1}$</td>
</tr>
<tr>
<td>$M_n$</td>
<td>$\int_0^\infty f(r) r^n dr$</td>
<td>m$^n$</td>
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<tr>
<td>$N$</td>
<td>concentration of droplets</td>
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</tr>
<tr>
<td>$N_1$</td>
<td>concentration of droplets before mixing</td>
<td>m$^{-3}$</td>
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<tr>
<td>$p$</td>
<td>pressure of moist air</td>
<td>N m$^{-2}$</td>
</tr>
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<td>$R_a$</td>
<td>specific gas constant of moist air</td>
<td>J kg$^{-1}K^{-1}$</td>
</tr>
<tr>
<td>$R_v$</td>
<td>specific gas constant of water vapor</td>
<td>J kg$^{-1}K^{-1}$</td>
</tr>
<tr>
<td>RH</td>
<td>$e / E_s$, relative humidity over water (saturation ratio)</td>
<td>-</td>
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\( RH_1 \) initial relative humidity in the cloud volume \((RH_1=1)\) - 
\( RH_2 \) relative humidity in the entrained sub-saturated parcel - 
\( RH_{m0} \) relative humidity after instant mixing of cloudy and entrained air but before droplets evaporation - 
\( q \) cloud liquid water mixing ratio (mass of liquid water per 1kg of dry air) - 
\( q_1 \) cloud liquid water mixing ratio before mixing - 
\( q_v \) water vapor mixing ratio (mass of water vapor per 1kg of dry air) - 
\( S \) \( e/e_s - 1 \), supersaturation - 
\( S_2 \) supersaturation of the dry out-of-cloud air - 
\( S_{m0} \) supersaturation after instant mixing of cloudy and entrained air, but before droplets start evaporating 

\( T \) temperature \( K \) 
\( T_1 \) temperature of the cloud parcel before mixing \( K \) 
\( T_2 \) temperature of the entrained sub-saturated parcel before mixing \( K \) 
\( T_{m0} \) temperature of the parcel after vapor mixing, but before droplet evaporation \( K \) 
\( \beta \) extinction coefficient \( m^{-1} \) 
\( \beta_1 \) extinction coefficient before mixing \( m^{-1} \) 
\( \delta q_m \) mixing ratio of liquid water required to saturate 1kg of the cloud volume after instant mixing, but before droplet evaporation. - 
\( \delta q^* \) mixing ratio of liquid water required to saturate 1kg of the dry out-of-cloud air - 
\( \mu \) cloud fraction of mixing air, \( 0 \leq \mu \leq 1 \) - 
\( \mu_{cr} \) critical cloud fraction, such that for \( \mu \leq \mu_{cr} \), all droplets evaporate - 
\( \rho_a \) density of the dry air \( \text{kg m}^{-3} \) 
\( \rho_w \) density of liquid water \( \text{kg m}^{-3} \) 
\( \xi \) coefficient \( 0 \leq \xi \leq 1 \) characterizing proximity of homogeneous mixing to inhomogeneous (when \( \xi \to 0 \)). - 

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Figure Captions

Figure 1. Classical conceptual diagram of (a) inhomogeneous and (b) homogeneous mixing. 1 initial state; 2 mixing state; 3 final state.

Figure 2. Dependence of critical mixing fraction $\mu_{cr}$ versus mixing ratio $q_0$ calculated from Eq.(7). Circles indicate modeled points. The calculations were performed for $T=0C$ and $H=3000m$.

Figure 3. Dependence of $\xi$ versus $\mu$. Numbers are the dimensionless ratios $\delta q^*/q_1$. Critical mixing ratios $\mu_{cr}$ are indicated by stars. Grey area indicates area where the moments of homogeneous and extreme inhomogeneous mixing may not be segregated from in-situ measurements. Dashed line was calculated for the cloud in Figs.13-14.

Figure 4. Simulation of (a) liquid water mixing ratio, (b) droplet number concentration, (c) integral droplet diameter, (d) extinction coefficient, (e) mean volume diameter, (f) time of phase relaxation, (g) relative humidity in the mixed volume before droplet evaporation $RH_{m0}$ and at the equilibrium state $RH_m$, (h) final temperature $T_{m0}$ versus ratio of mixing $\mu$ formed after homogeneous and extreme inhomogeneous mixing between dry and cloudy parcel with monodisperse droplets. Black stars indicate critical mixing fraction $\mu_{cr}$ calculated from Eq.(7). The calculations were performed for $RH_2 =0.2, 0.5, 0.8, 0.95; D_1=20\mu m, N_1=500cm^{-3}; T_1= T_2 =0C; H=1000m$.

Figure 5. Dependence of normalized liquid water mixing ratio $q/q_1$ (a,d,g), extinction coefficient $\beta/\beta_1$ (b,e,h) and mean volume diameter $D_v/D_v1$ (c,f,j) versus normalized number concentration $N/N_1$ for various humidity of the entrained air (a,b,c), for various liquid water mixing ratios (d,e,f) and for various temperatures (g,h,j). The calculations were performed the initial conditions: $H=1000m, D_1=20\mu m; (a-c; g-j) N_1=500cm^{-3}; (a-f) T_1 = T_2 =0C$.

Figure 6. Simulation of (a) droplet number concentration and (b) liquid water mixing ratio, (c) integral droplet diameter, (d) extinction coefficient, (e) mean volume diameter, (f) time of phase relaxation, (g) relative humidity in the mixed volume before droplet evaporation $RH_{m0}$ and at the equilibrium state $RH_m$, (h) final temperature $T_m$ versus ratio of mixing $\mu$ formed after homogeneous and extreme inhomogeneous mixing between dry and cloudy
parcel with monodisperse droplets. The calculations were performed for \( RH_2 = 0.9; \)

\( D_1 = 10 \mu m, N_1 = 500 \text{cm}^{-3}; T_1 = 0 \text{C}; T_2 = -10 \text{C}, -5 \text{C}, 0 \text{C}; H = 1000 \text{m}. \)

**Figure 7.** Effect of temperature difference between cloud and entrained air on mixing. The calculations were performed for initial temperatures \( T_2: \) (1) -10°C; (2) -5°C; (3) 0°C. Grey circles indicate extreme inhomogeneous mixing on line 1 at the \( AB \) interval. The rest cases on extremely inhomogeneous mixing are indicated by open circles. The initial conditions used for the calculations were: \( H = 1000 \text{m}, RH_2 = 90\%; D_1 = 10 \mu m, N_1 = 500 \text{cm}^{-3}, T_1 = 0 \text{C}. \)

**Figure 8.** Conceptual diagram of cascade mixing of the out-of-cloud entrained parcel with the cloudy environment

**Figure 9.** Simulation of stochastic mixing corresponding to stages 1-4 as indicated in Fig.8. Solid red lines indicate the normalized dependences \( q, \beta, D_v \) vs. \( N \) for the primary stage of homogeneous mixing. Dashed red lines indicate the same dependences for inhomogeneous mixing. The initial conditions used for the simulations were: \( H = 1000 \text{m}, T_1 = T_2 = 0 \text{C}; RH_2 = 0.5; D_1 = 10 \mu m, N_1 = 500 \text{cm}^{-3}. \)

**Figure 10.** Conceptual diagram explaining breaking the functional relationships between the microphysical moment during progressive missing (see text).

**Figure 11.** Droplet size distributions formed during the progressive homogeneous mixing corresponding to the (a,e) primary stage; (b,f) 2nd stage; (c,g) 3rd stage; (d,h) 4th stage. Left column (a,b,c,d) corresponds to the case, when the cloud temperature is equal to the dry air temperature \( T_1 = T_2 = 0 \text{C}. \); right column (e,f,g,h) corresponds to the case when \( T_1 = 0 \text{C}, T_2 = -10 \text{C}. \) For both cases the simulation was performed for \( D_1 = 10 \mu m; N = 500 \text{cm}^{-3}; RH_2 = 0.9. \)

**Figure 12.** Conceptual diagrams of scattering of measurements of \( q \) versus \( N \) for (a) extreme inhomogeneous and (b) homogeneous mixing.

**Figure 13.** Spatial changes of particle concentration (a), extinction coefficient (b), liquid water content (c) and average and mean mass diameter (d) during transit through one of the convective clouds measured by CDP. The measurements were conducted during the COPE-MED project on 18 July, 2015. The sampling rate 10Hz (~10m spatial resolution). \( H = 5500 \text{m}, T = -12 \text{C}, RH = 0.2. \)

**Figure 14.** Relationships between (a) \( LWC(N) \); (b) \( \beta(N) \); (c) \( D_v(N) \); (d) \( LWC(\beta) \) calculated from the CDP measurements obtained during sampling several convective clouds. The
measurements were conducted during the COPE-MED project on 18 July, 2015, $H=5500\text{m}$, $T=-12\text{C}$, $RH=0.2$. The measurements were sampled at 10Hz (~10m spatial resolution). Dashed lines are linear regressions. Red lines indicate primary inhomogeneous mixing dependencies calculated for the same environmental conditions.

**Figure 15.** Relationships between (a) $LWC(N)$; (b) $\beta(N)$; (c) $D_{\nu}(N)$; (d) $LWC(\beta)$ calculated from the CDP measurements sampled during traverse through 45 convective clouds. The measurements were conducted during the COPE-MED project on 02 August, 2015. Dashed lines indicate (a), (b) and (d) indicate the sectors, where the majority of the points are scattered. The altitude of sampling varied in the range $3000\text{m} < H < 4500\text{m}$, temperature $-11\text{C} < T < 0\text{C}$, relative humidity in the vicinity of clouds $15\% < RH < 65\%$. The measurements were sampled at 10Hz (~10m spatial resolution).

**Figure A1.** Amount of evaporated liquid water $\delta q_m$ required for saturation of a cloud volume with initial humidity $RH_m$. Comparisons of the modeled $\delta q_m$ and that calculated from Eqs. (A8) and (A9) for three temperatures $T_{m0} = -20\text{C}$, 0C and 20C. Calculations were performed for $P=880\text{mb}$. 
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