



Particle-area  
dependence of  
mineral dust in the  
immersion mode

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# Particle-area dependence of mineral dust in the immersion mode: investigations with freely suspended drops in an acoustic levitator

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## Abstract

The heterogeneous freezing temperatures of supercooled drops were measured by using an acoustic levitator. This technique allows to freely suspending single drops in air without electrical charges thereby avoiding any electrical influences which may affect the freezing process. Heterogeneous nucleation caused by several mineral dust particles (montmorillonite, two types of illite) was investigated in the immersion mode. Drops of 1 mm in radius were monitored by a video camera during cooling down to  $-28^{\circ}\text{C}$  to simulate the tropospheric temperature range. The surface temperature of the drops was remotely determined with an infra-red thermometer so that the onset of freezing was indicated. For comparisons, measurements with one particle type were additionally performed in the Mainz vertical wind tunnel with drops of  $340\ \mu\text{m}$  radius freely suspended. The data were interpreted regarding the particle surfaces immersed in the drops. Immersion freezing was observed in a temperature range between  $-13$  and  $-26^{\circ}\text{C}$  in dependence of particle type and surface area per drop. The results were evaluated by applying two descriptions of heterogeneous freezing, the stochastic and the singular model.

## 1 Introduction

The types and quantities of atmospheric ice nuclei affect ice cloud microphysical and radiative properties as well as their precipitation efficiency. This has been shown by model studies as, e.g., Phillips et al. (2007), Storelvmo et al. (2008), and Hoose et al. (2008). The role of mineral dust particles as ice nuclei is undoubted (e.g., Hoose and Möhler, 2012). The most abundant minerals occurring in desert aerosols are quartz, calcite, mica, hematite, illite, and gypsum (Kandler et al., 2007). So far, laboratory experiments of heterogeneous freezing have been performed mainly with kaolinite, montmorillonite, and illite (e.g., Hoffer, 1961; Pitter and Pruppacher, 1973; Murray et al., 2011; Pinti et al., 2012; Broadley et al., 2012), and Arizona test dust or

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## 3 Results and discussion

### 3.1 Frozen fractions and median freezing temperatures

#### 3.1.1 Results from acoustic levitator experiments

The particles immersed in the drops were evaluated in terms of particle surface area per drop. These were calculated from the particle concentrations in the stock solution and the average drop size. With illite IMt1 and illite NX particles, three different particle concentrations were investigated, with montmorillonite K10 only one particle concentration. Two illite NX particle concentrations were investigated at the vertical wind tunnel also. The cases are listed in Table 1.

The results indicate that immersion freezing is dependant on the particle surface area in the drop. This confirms the findings of other recent studies as, e.g., Murray et al. (2011), Hartmann et al. (2013), and Broadley et al. (2012). In the following Figs. 6 to 8, same colours represent data for similar particle surface areas per drop. Figures 6 and 7 show the fractions of frozen drops as function of temperature for illite IMt1 and illite NX, respectively, as measured in the acoustic levitator. With decreasing particle surface areas in the drops the median freezing temperature decreases, too, but the differences are reduced towards lower particle surface areas, see Table 1. In case of illite IMt1, the median freezing temperature decreased from  $-18.8^{\circ}\text{C}$  to  $-23.6^{\circ}\text{C}$  when the particle surface area per drop was reduced by one order of magnitude; in case of illite NX,  $T_{50}$  decreased from  $-19.7^{\circ}\text{C}$  to  $-23.7^{\circ}\text{C}$  by reducing the particle surface area per drop by two orders of magnitude. Differences between the two illite types with comparable particle surface areas are not significant as they are only slightly higher than the measurement accuracies ( $\pm 0.7\text{K}$ ): the median freezing temperatures of illite IMt1 are  $-23.6 \pm 0.7^{\circ}\text{C}$  and  $-18.8 \pm 0.7^{\circ}\text{C}$  for particle surface areas of  $3.5 \times 10^{-6} \text{m}^2 \text{drop}^{-1}$  and  $7.0 \times 10^{-5} \text{m}^2 \text{drop}^{-1}$ , respectively, for illite NX median freezing temperatures of  $-22.8 \pm 0.7^{\circ}\text{C}$  and  $-19.7 \pm 0.7^{\circ}\text{C}$  were measured for particle concentrations of  $7.1 \times 10^{-6} \text{m}^2 \text{drop}^{-1}$  and  $7.1 \times 10^{-5} \text{m}^2 \text{drop}^{-1}$ , respectively.

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derived that

$$\ln \frac{n_{\text{liq}}}{N_{\text{total}}} = -J(T) s t \quad (5)$$

and the results are given in Figs. 14 and 15 for  $5.1 \times 10^{-6} \text{ m}^2$  per drop and  $5.1 \times 10^{-5} \text{ m}^2$  per drop, respectively, for different temperatures. Cases where freezing took place during the cooling stage of the drops were not considered, that means freezing events during the first 4 s (i.e. on the left-hand-side of the vertical line in the figures). One can note that except for one case (at  $-21 \text{ }^\circ\text{C}$  with  $s = 5.1 \times 10^{-6} \text{ m}^2$  per drop) the data very well follow straight lines indicating the exponential decay of the liquid drops with time at constant temperatures as predicted by Eq. (5). This confirms that nucleation events during the wind tunnel experiments were stochastic processes affected by a single nucleation site type.

To apply the stochastic model to the data measured with the acoustic trap one has to consider the effect of the non-linear cooling rate. For that purpose Eq. (4) was modified as follows. It was assumed that during temperature changes of 1 K the cooling rate was nearly constant. For each temperature in steps of 1 K the total cooling time  $t$  was calculated according to Eq. (1). Afterwards, for each temperature change  $\Delta T$  the required time  $\Delta t$  was calculated and the cooling rate  $\gamma(T)$  was determined from

$$\gamma(T) = \frac{\Delta T}{\Delta t} \quad (6)$$

with  $\Delta T = 1 \text{ K}$ . Thus, for a temperature change from  $T_1$  to  $T_2$  there is a cooling rate according to Eq. (6) and the change of the frozen fraction is given by

$$\Delta \left( \frac{n_f}{N_{\text{total}}} \right) = \frac{\Delta n_f}{N_{\text{total}}} = \frac{n_{f,2}}{N_{\text{total}}} - \frac{n_{f,1}}{N_{\text{total}}} \quad (7)$$

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considering that  $N_{\text{total}}$  is constant. Analogue to Eq. (2), the number of drops  $\Delta n_{\text{fr}}$  freezing heterogeneously during a temperature change  $\Delta T$  is given by

$$\Delta n_f = N_{\text{total}} \left( 1 - \exp \left( -J(T) s \Delta T \frac{1}{\gamma(T)} \right) \right) \quad (8)$$

5 with the cooling rate  $\gamma$  in units of  $[\text{K s}^{-1}]$  and the nucleation rate coefficient  $J(T)$  in units of  $[\text{area}^{-1} \text{s}^{-1}]$ . Thus,  $J(T)$  can be calculated by

$$J(T) = - \frac{\ln \left( 1 - \Delta \frac{n_n}{N_{\text{total}}} \right)}{s \Delta T \frac{1}{\gamma(T)}} \quad (9)$$

with  $\Delta T = 1 \text{ K}$ .

10 A comparison of the nucleation rate coefficients derived from acoustic levitator and wind tunnel measurements is given in Fig. 16. Results from wind tunnel experiments (derived according to Eq. 4) are shown with their regression line (solid line in black) as in Fig. 13. The dotted black line gives the extrapolation of the regression line towards higher and lower temperatures. Results from acoustic trap experiments were calculated  
15 by using the modified Eq. (9). They show a rather large scatter around the regression line; however, in the temperature range below  $-17^\circ\text{C}$  they follow the same trend. At higher temperatures the data are located definitely above the extrapolated regression line. This indicates that in the acoustic levitator experiments the freezing rate of the drops during the first 15 s of cooling is overestimated because of the very fast cooling rate in the beginning.  
20

### 3.2.2 Singular model

Besides the stochastic model, it is suggested that heterogeneous freezing is dominated by the nucleating characteristics of ice-active sites and, thus, only dependant on temperature while the time-dependence, i.e. the stochastic nature of the freezing







techniques within the frame work of INUIT. A compilation of all results from the entire INUIT community with a general parameterization applicable to model simulations will be presented in a future joint publication.

In spite of some deficiencies the use of the acoustic levitator has a number of essential advantages. It is a small transportable instrument and can be easily installed. It does not require a huge amount of air flow and, thus, energy to establish drop floating and is, therefore, much more economical in its operation. Although in the present experiments the levitator was placed inside a walk-in cold chamber, it might as well be placed inside a table top cold box. The possibility to directly measure the drop temperature with an infra-red thermometer allows to clearly defining the onset of freezing. In particular for nucleation processes, flow hydrodynamics and ventilated heat transfer as it happens in the wind tunnel are not deciding factors as much as the temperature and the cooling rate. If required, a small design modification could bring additional ventilated heat transfer. Thus, the acoustic levitator presents a good alternative to other methods to investigate drop freezing in the immersion mode.

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**Figure 1.** Acoustic levitator.

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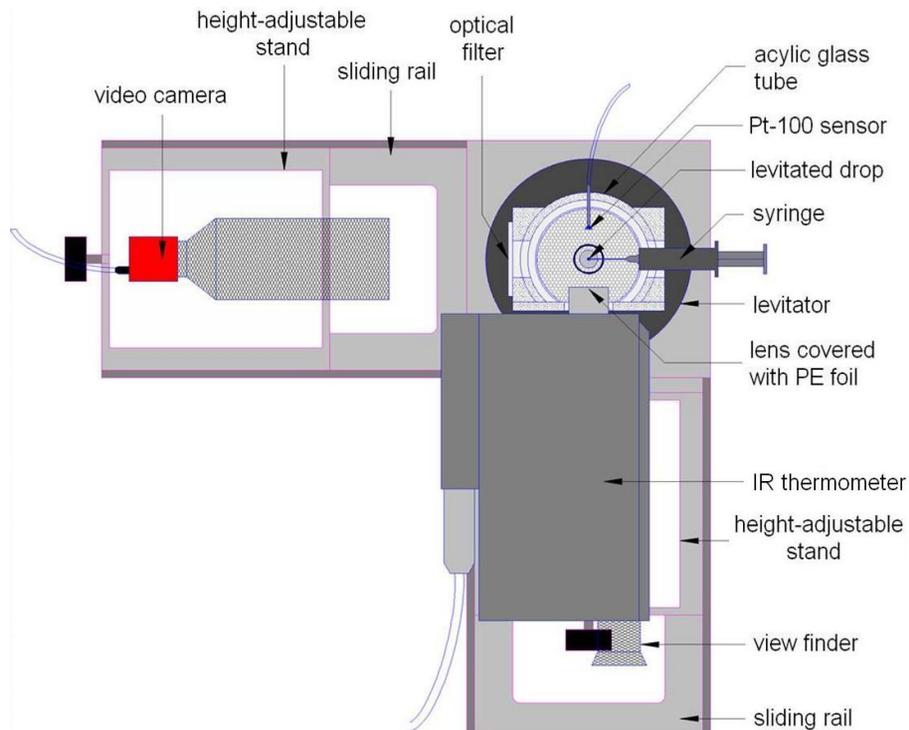
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**Figure 2.** Scheme of the experimental setup with the acoustic trap in the cold chamber.

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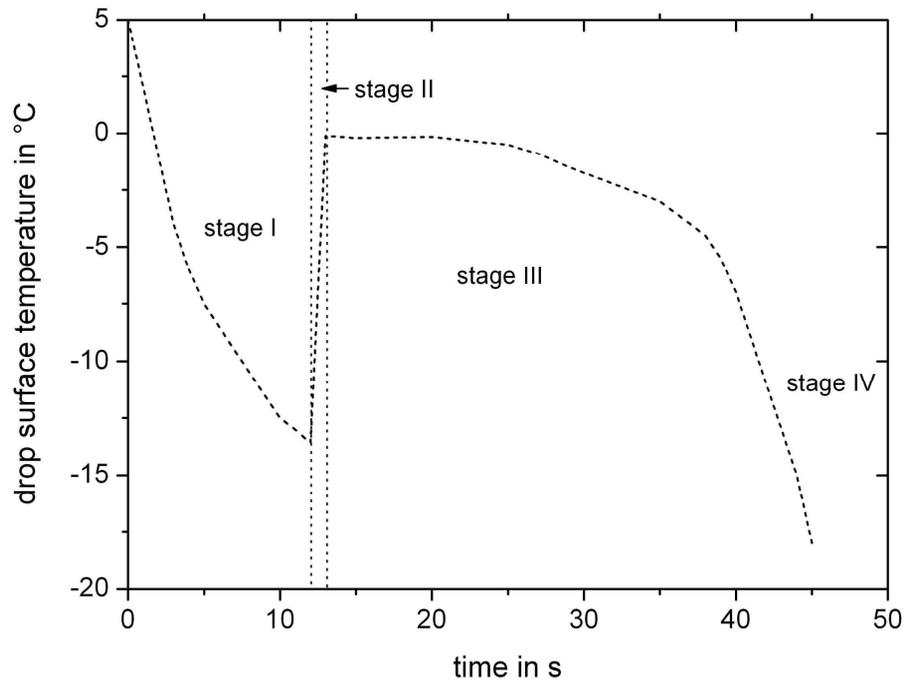
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**Figure 3.** Example of the development of the drop temperature with time during freezing.

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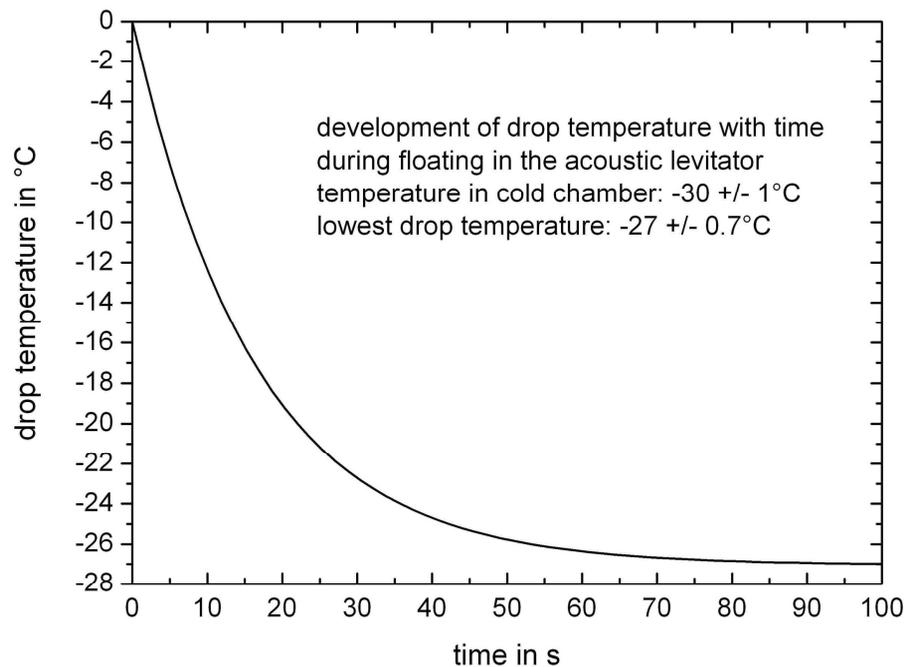
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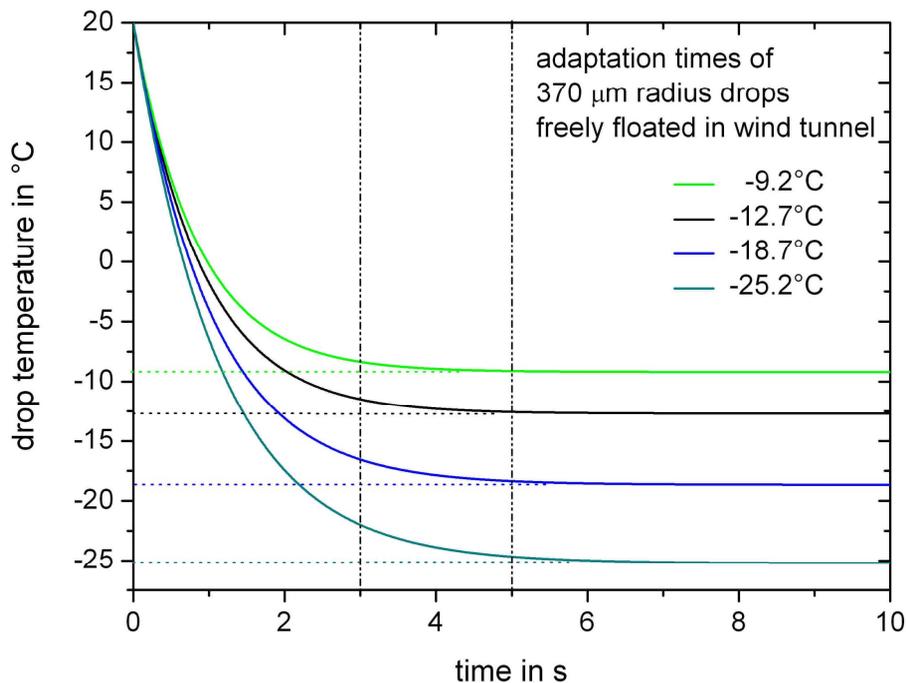


**Figure 4.** Development of drop temperature during freely floating in the acoustic levitator at a cold chamber ambient temperature of  $-30^\circ\text{C}$ .

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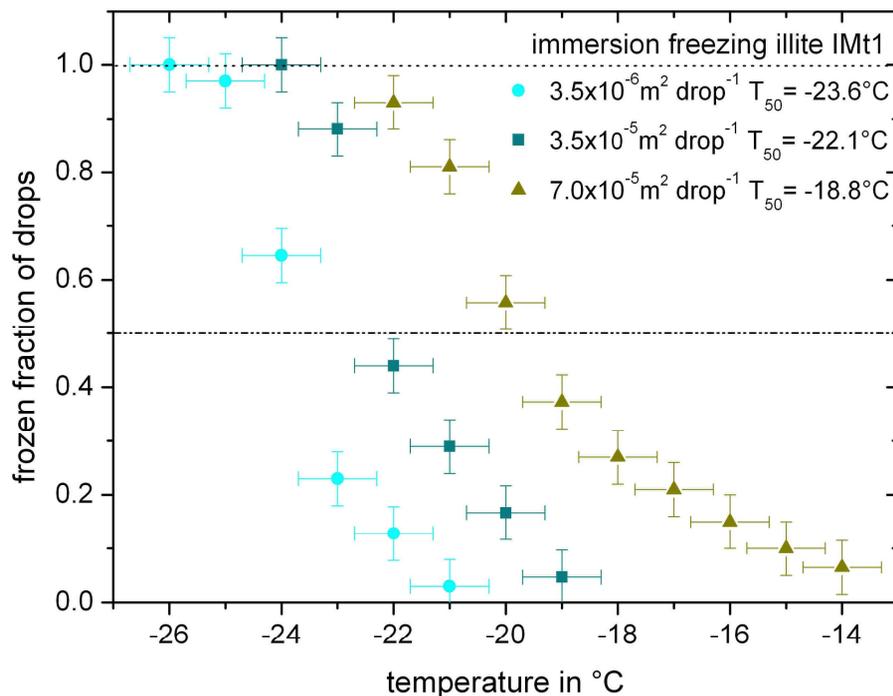


**Figure 5.** Calculated adaptation times of 370 radius drops while freely floating in the wind tunnel at various ambient temperatures.

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**Figure 6.** Immersion freezing of illite IMt1 in the acoustic levitator: frozen fraction of drops as function of temperature for three different particle surface areas per drop.

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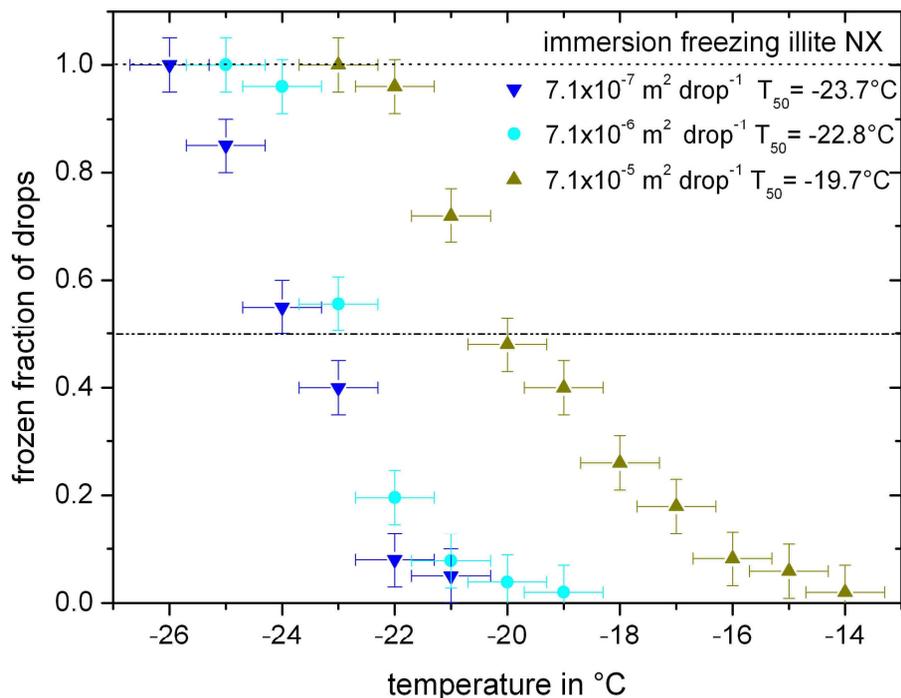
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**Figure 7.** Immersion freezing of illite NX in the acoustic levitator: frozen fraction of drops as function of temperature for three different particle surface areas per drop.

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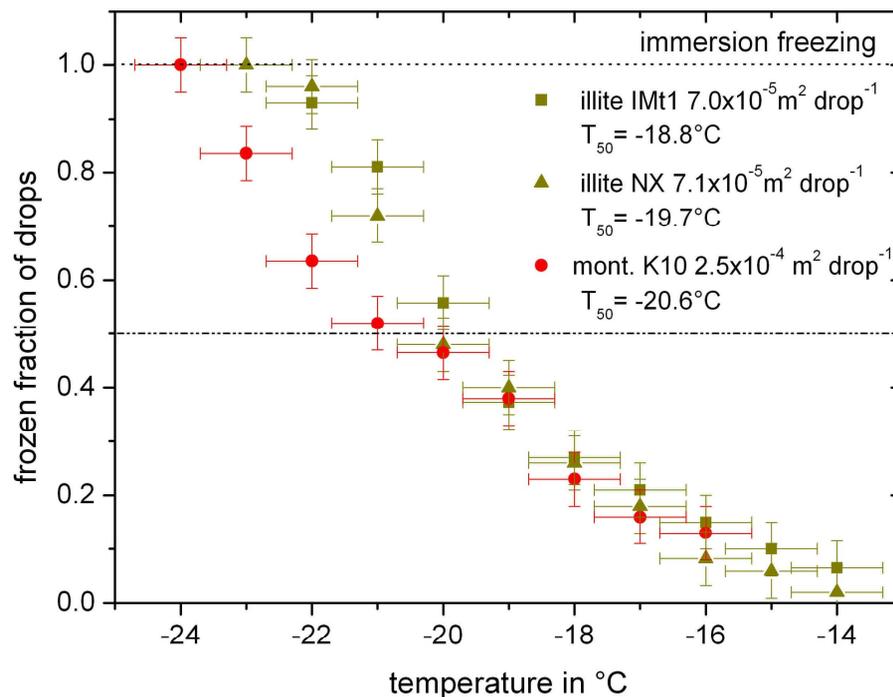
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**Figure 8.** Immersion freezing for montmorillonite K10 in comparison to illite: frozen fraction of drops as function of temperature.

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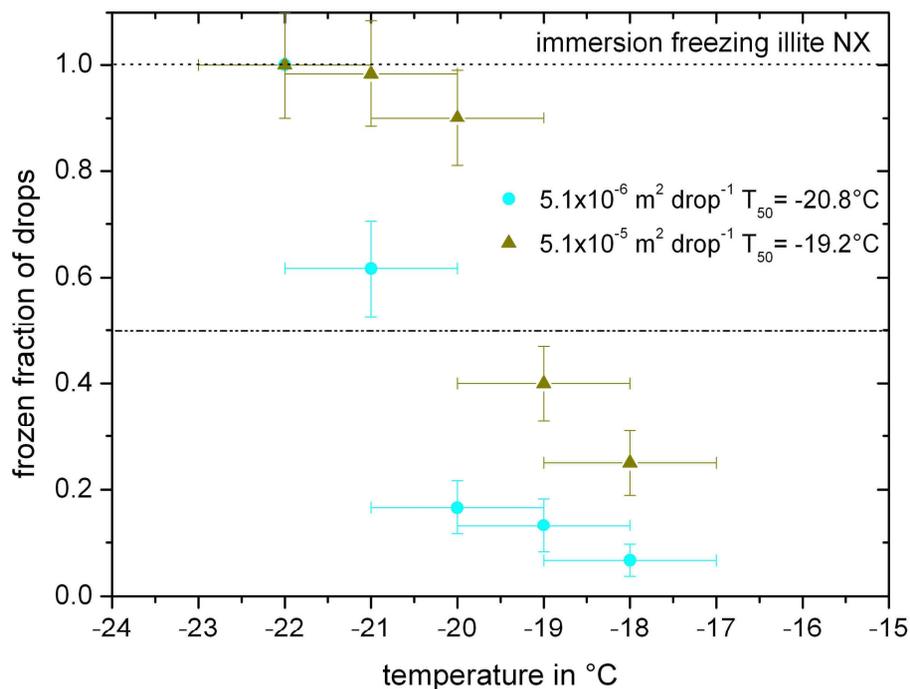
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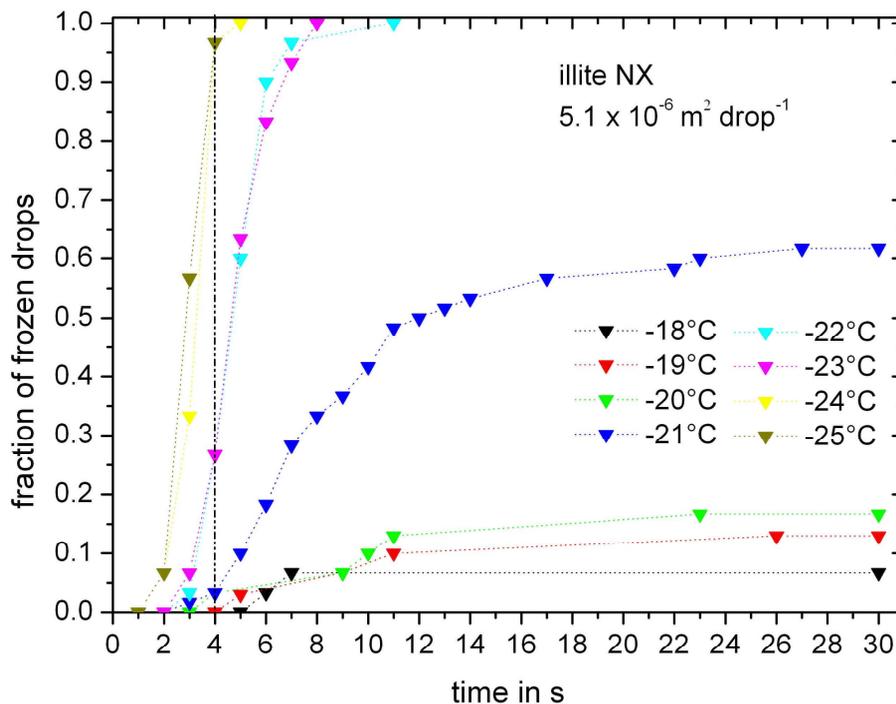
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**Figure 9.** Immersion freezing of illite NX in the wind tunnel: frozen fraction of drops as function of temperature for two different particle surface areas per drop. Accumulated values within total observation time of 30 s.

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**Figure 10.** Time resolved frozen fractions measured in the wind tunnel with illite NX present with  $5.1 \times 10^{-6} \text{ m}^2$  per drop at different temperatures.

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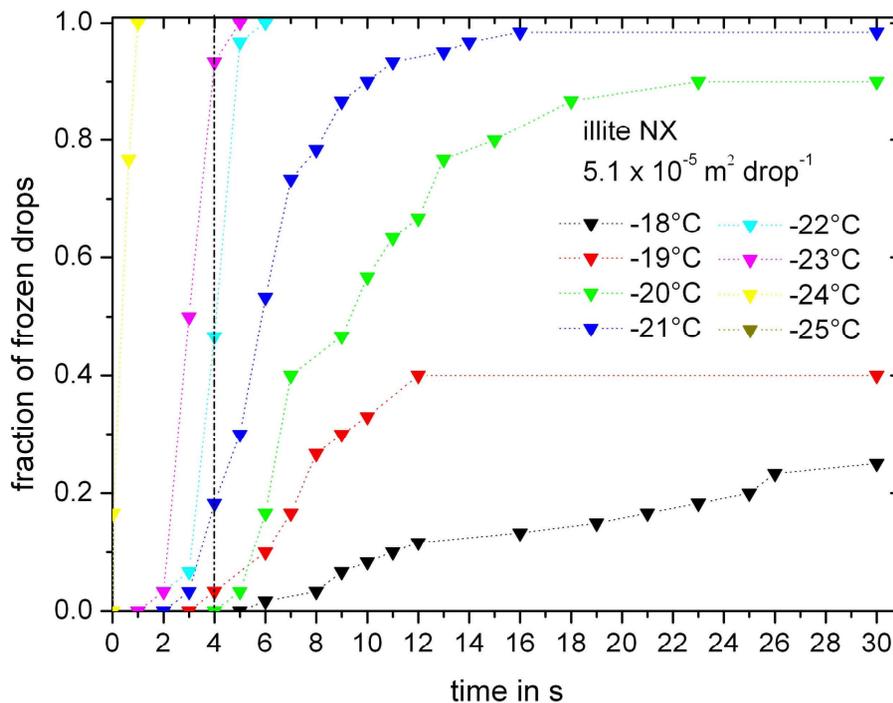
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**Figure 11.** Time resolved frozen fractions measured in the wind tunnel with illite NX present with  $5.1 \times 10^{-5} \text{ m}^2$  per drop at different temperatures.

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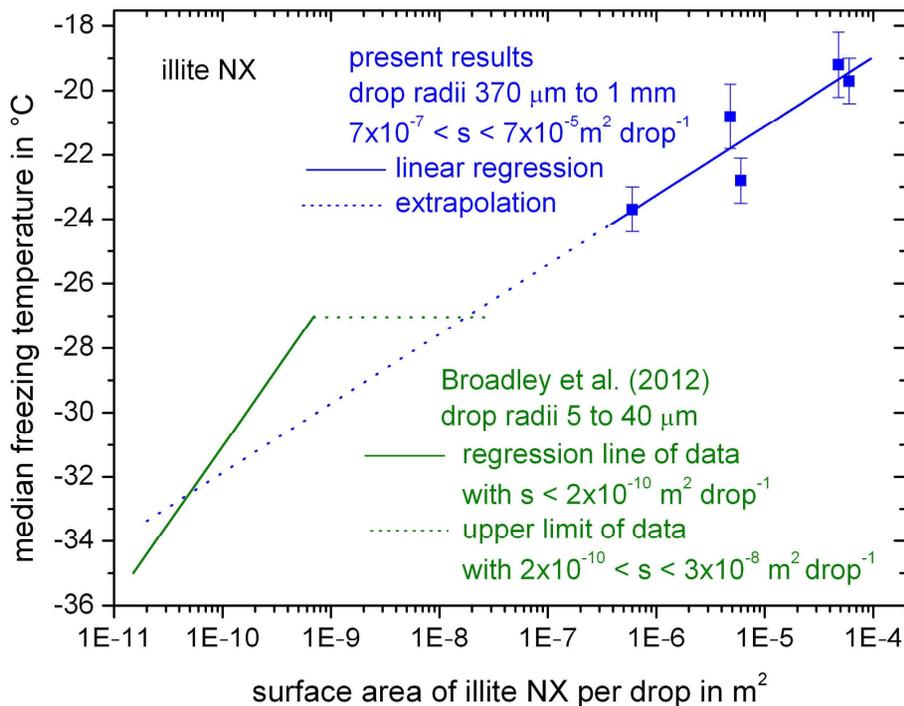
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**Figure 12.** Median freezing temperatures of illite for various surface areas per drop. Solid blue line with symbols: present experiments from acoustic levitator and wind tunnel, dotted blue line: extrapolation. Green: results from Broadley et al. (2012).

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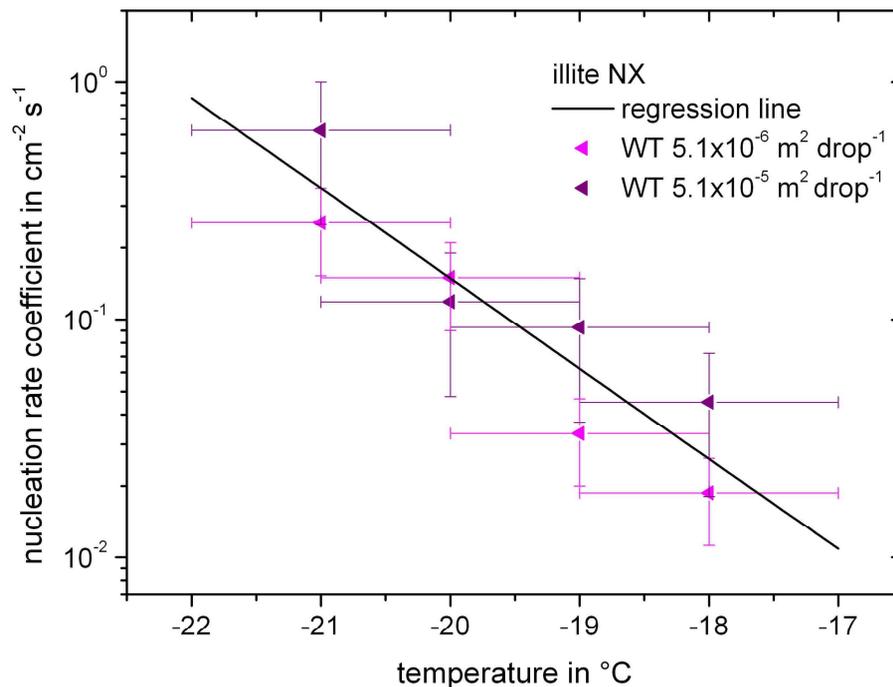
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**Figure 13.** Nucleation rate coefficients as function of temperature for illite NX for two particle surface areas per drop, investigated in the wind tunnel.

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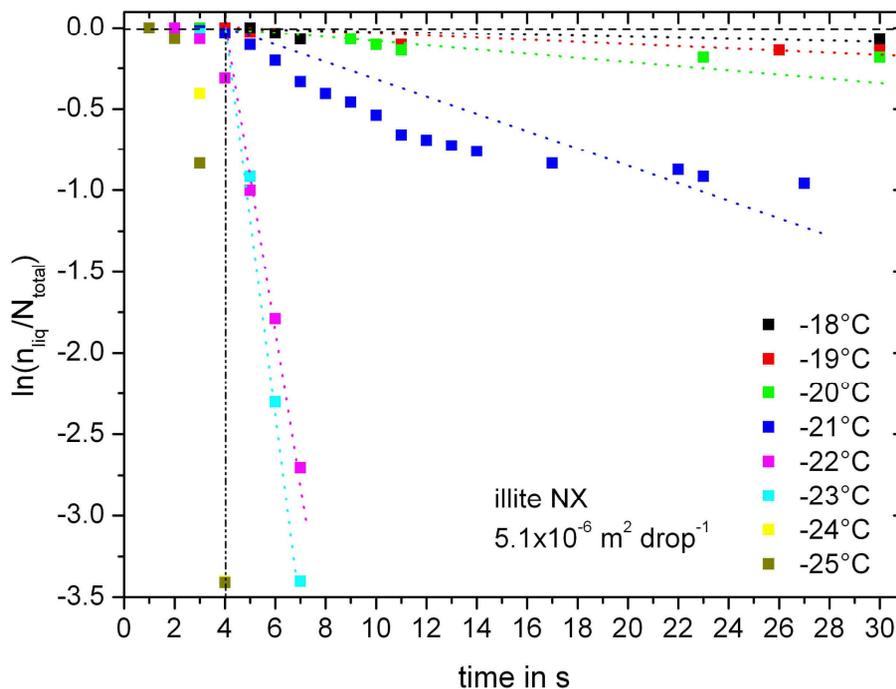
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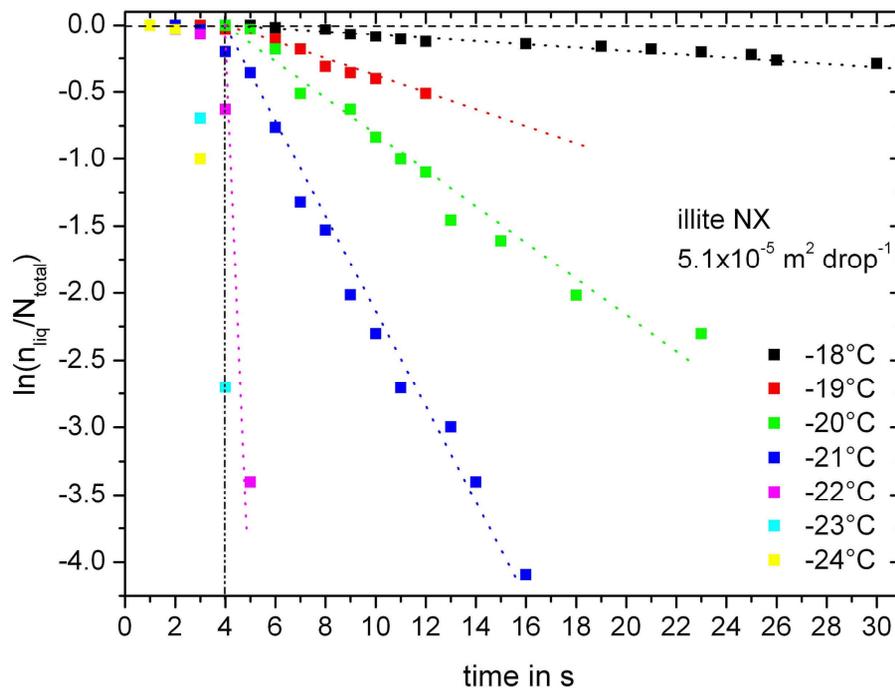
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**Figure 14.** Liquid ratio as function of time from wind tunnel experiments at different temperatures, illite NX present with  $5.1 \times 10^{-6} \text{ m}^2$  per drop. Vertical line: limit of adaptation time of the drops.

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**Figure 15.** Liquid ratio as function of time from wind tunnel experiments at different temperatures, illite NX present with  $5.1 \times 10^{-5} \text{ m}^2$  per drop. Vertical line: limit of adaptation time of the drops.

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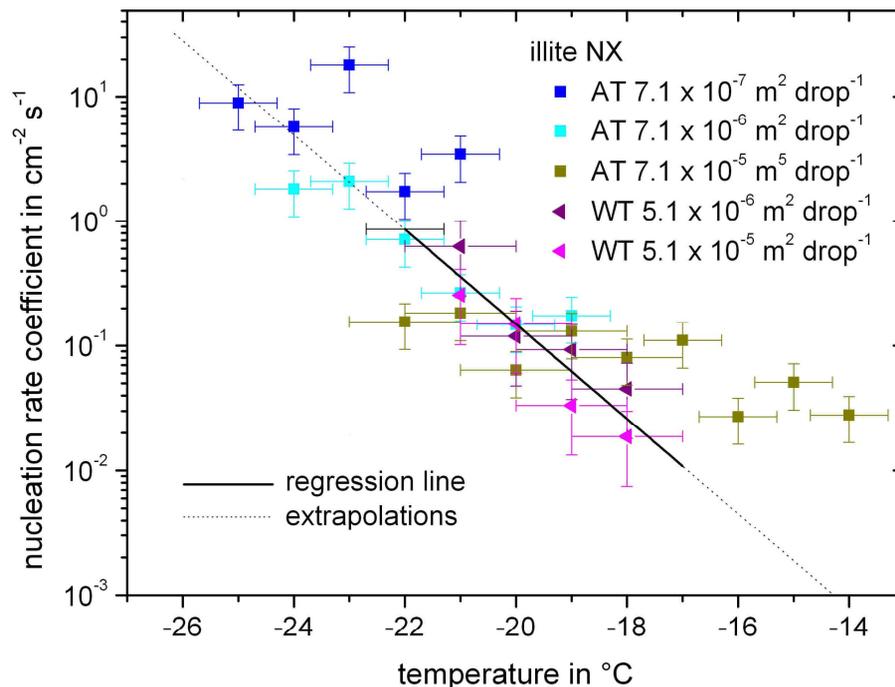
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**Figure 16.** Nucleation rate coefficients as function of temperature for illite NX for various particle surface areas per drop, determined by two experimental techniques.

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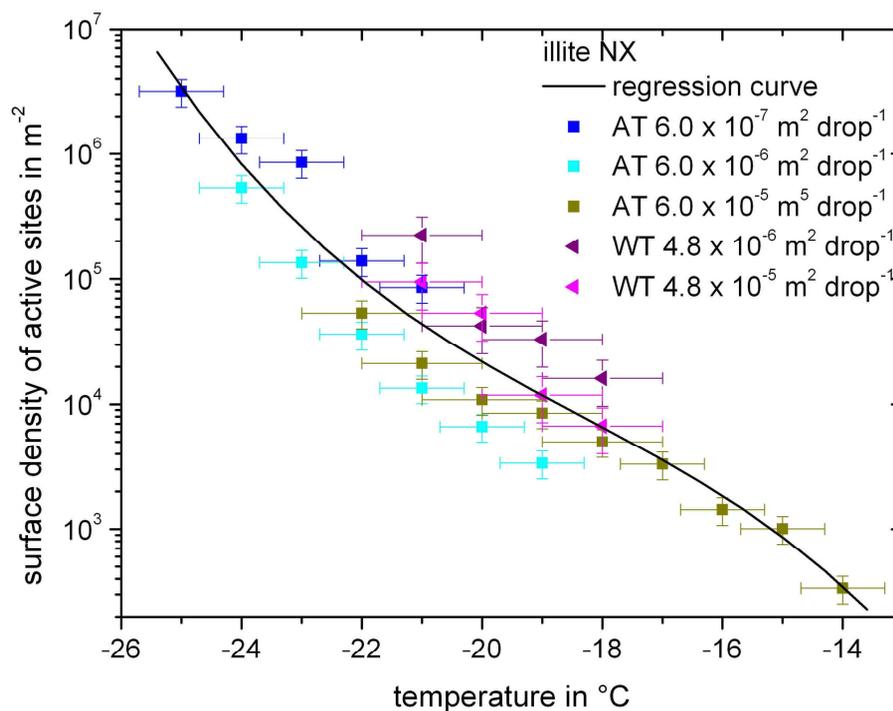
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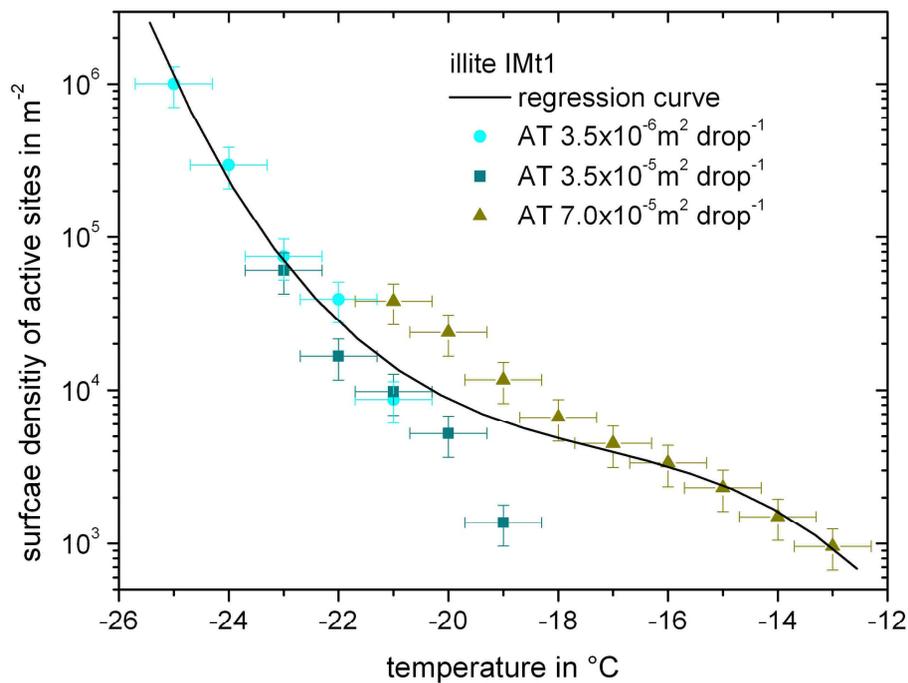
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**Figure 17.** Surface density of illite NX as function of temperature for various particle surface areas per drop, determined by two experimental techniques.

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**Figure 18.** Surface density of illite IMt1 as function of temperature for various particle surface areas per drop, determined by the acoustic levitator.

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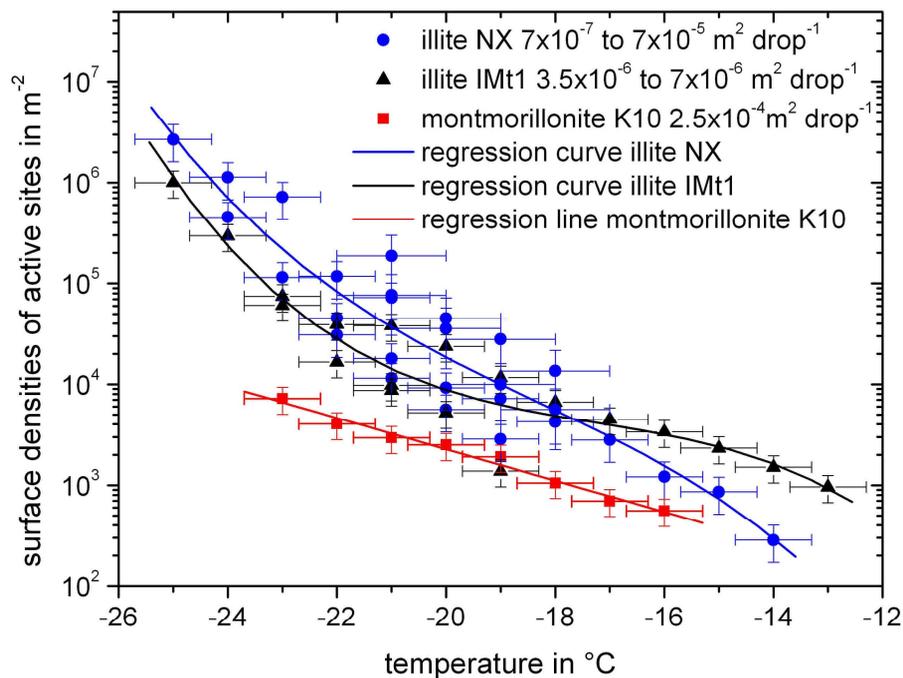
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**Figure 19.** Comparison of the surface densities of illite NX and IMt1.

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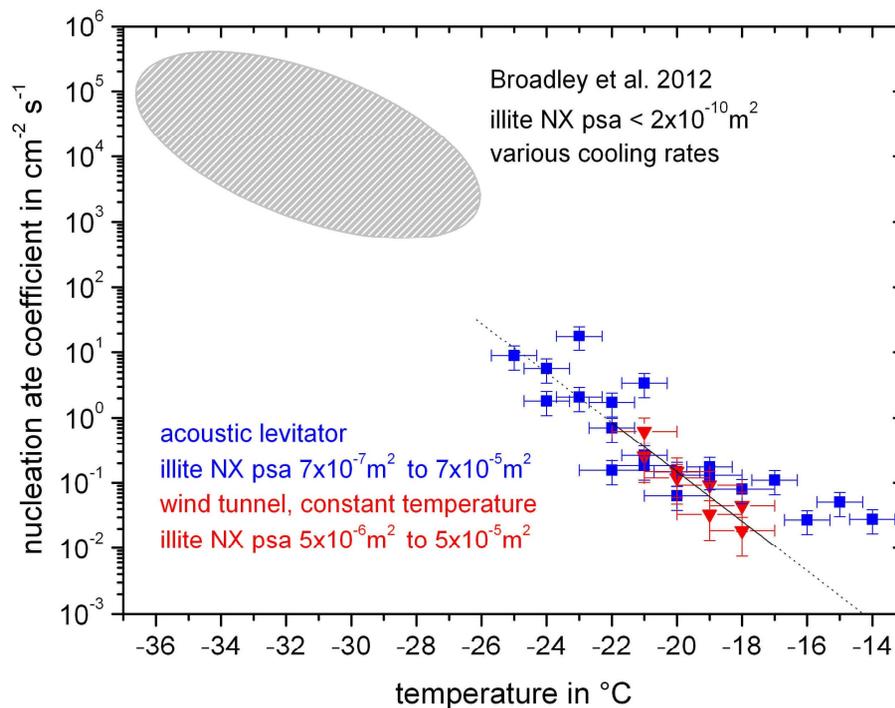
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**Figure 20.** Nucleation rate coefficients for illite NX derived from present (shown in blue and red) and previous experiments (indicated as grey region, from Broadley et al., 2012).

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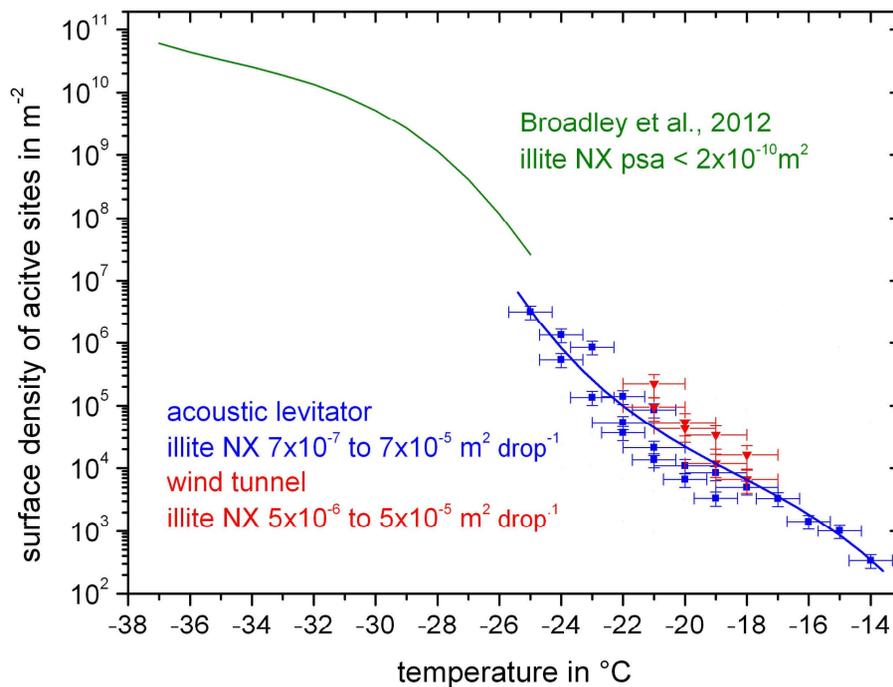
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**Figure 21.** Surface densities of active sites for illite NX derived from present (shown in blue and red) and previous experiments (shown in green, from Broadley et al., 2012).